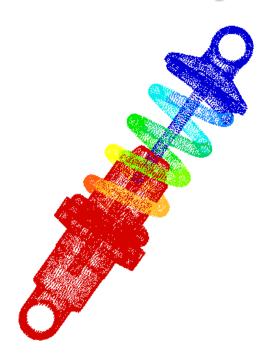
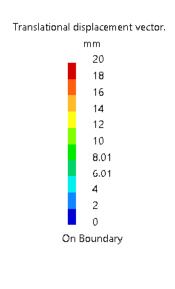
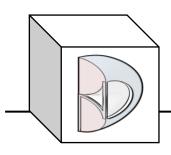




Shock Absorber Preload Analysis using CATIA Generative Structural Analysis (FEA)

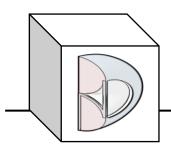






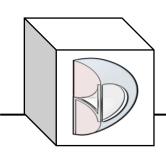


- The following licenses are required to create the Shock Absorber Preload Simulation:
 - Generative Shape Design
 - Mechanical Part Design
 - Generative Structural Analysis





- Issues to prove with this coil over shock absorber FEA analysis:
 - 1. The spring rate will be linear when the spring has a consistent (evenly spaced) pitch and a constant diameter.
 - Preloading the spring on the coil over assembly will NOT change the rate of the spring.
 - 3. Preloading the spring on the coil over assembly WILL affect the deflection at load (length at load) of the shock absorber.





1.1) Calculate the spring values.

From CATIA				C3 Project Front Spring Calculation												
		Poisson's ratio (v) [transverse	Modulus of Rigidity (G)		Wire Diameter [d]		Spring Mean Diameter [D]			Free Length [L _f]			Total coils [N _t]	Active coils [N _a]	Select End Types:	
(psi x 10 ⁶)	(MPa x	contraction	(psi x 10 ⁶)	(MPa x 10 ³)	inch	m	mm	inch	m	mm	inch	m	mm	value	value	Choice
30.0	207.0	0.305	11.5	79.3	0.500	0.0127	12.7	3.000	0.0762	76.2	10.000	0.254	254	8.650	6.650	Squared or closed (Ground)
	Young's M [modulus o (psi x 10 ⁶)	Young's Modulus (E) [modulus of elasticity] (psi x 10 ⁶) (MPa x	Young's Modulus (E) (ν) [modulus of elasticity] (psi x 10 ⁶) (MPa x	Young's Modulus (E) (v) Modulus (c) (transverse (psi x 10 ⁶) (MPa x (psi x 10 ⁶) (psi x 10 ⁶)	Young's Modulus (E) Poisson's ratio (v) Modulus of Rigidity (G) [modulus of elasticity] [transverse contraction (psi x 10 ⁶) (MPa x 10 ³) (MPa x 10 ³) 30.0 207.0 0.305 11.5 79.3	Young's Modulus (E) [modulus of elasticity] Poisson's ratio (v) [transverse contraction 30.0 Modulus of Rigidity (G) D (psi x 10 ⁶) (MPa x contraction 0.305 (psi x 10 ⁶) (MPa x 10 ³) inch 30.0 207.0 0.305 11.5 79.3 0.500	Young's Modulus (E) [modulus of elasticity] Poisson's ratio (ν) [transverse ocntraction 30.0 Modulus of Rigidity (G) Wire Diameter [Modulus of Rigidity (G)] (psi x 10 ⁶) (MPa x contraction 30.0 (psi x 10 ⁶) (MPa x 10 ³) inch m inch m 30.0 207.0 0.305 11.5 79.3 0.500 0.0127	Young's Modulus (E) [modulus of elasticity] Poisson's ratio (v) [transverse contraction 30.0 Modulus of Rigidity (G) Wire Diameter [d] (psi x 10 ⁶) (MPa x contraction 30.0 (psi x 10 ⁶) (MPa x 10 ³) inch m mm m 30.0 207.0 0.305 11.5 79.3 0.500 0.0127 12.7	Young's Modulus (E) [modulus of elasticity] Poisson's ratio (v) [transverse ontraction 30.0 Modulus of Rigidity (G) Wire Diameter [d] Sp Diameter [d] (psi x 10 ⁶) (MPa x contraction 30.0 (psi x 10 ⁶) (MPa x 10 ³) inch m mm inch mm inch 30.00 inch 30.00 0.0127 12.7 3.000	Young's Modulus (E) [modulus of elasticity] Poisson's ratio (v) [transverse Modulus of Rigidity (G) Wire Diameter [d] Spring Mean Diameter [D] (psi x 10 ⁶) (MPa x contraction 30.0 207.0 0.305 11.5 79.3 0.500 0.0127 12.7 3.000 0.0762	Young's Modulus (E) [modulus of elasticity] Poisson's ratio (v) [transverse contraction 30.0 Modulus of Rigidity (G) Wire Diameter [d] Spring Mean Diameter [D] (psi x 10 ⁶) (MPa x 10 ⁶) (MPa x 10 ³) inch m mm inch m mm inch m mm m mm inch m mm m mm 30.0 207.0 0.305 11.5 79.3 0.500 0.0127 12.7 3.000 0.0762 76.2	Young's Modulus (E) [modulus of elasticity] Poisson's ratio (v) [transverse contraction 30.0 Modulus of Rigidity (G) Wire Diameter [d] Spring Mean Diameter [D] Free Diameter [D] (psi x 10 ⁶) (MPa x 10 ⁶) (MPa x 10 ³) inch m mm inch m m mm inch m m mm inch m m mm inch m m mm inch m m m m m m m m m m m m m m m m m m m	Young's Modulus (E) [modulus of elasticity] Poisson's ratio (v) [transverse ontraction 30.0 Modulus of Rigidity (G) Wire Diameter [d] Spring Mean Diameter [D] Free Length [L ₁] (psi x 10 ⁶) (MPa x contraction 30.0 (psi x 10 ⁶) (MPa x 10 ³) inch m mm inch m inch inch m inch inch m inch inch inch inch inch inch inch inch	Young's Modulus (E) [modulus of elasticity] Poisson's ratio (v) [transverse ontraction 30.0 Modulus of Rigidity (G) Wire Diameter [d] Spring Mean Diameter [D] Free Length [L] (psi x 10 ⁶) (MPa x 00 ⁶) (MPa x 10 ⁶) (MPa x 10 ⁶) (MPa x 10 ⁶) m mm inch m mm inch m mm inch m mm m mm 30.0 207.0 0.305 11.5 79.3 0.500 0.0127 12.7 3.000 0.0762 76.2 10.000 0.254 254	Young's Modulus (E) [modulus of elasticity] Poisson's ratio (v) [transverse contraction 30.0 Modulus of Rigidity (G) Wire Diameter [d] Spring Mean Diameter [D] Free Length [L-] Total coils [N,] (psi x 10 ⁶) (MPa x 20 ³) (mpi x 10 ⁶) (MPa x 10 ³) inch m mm inch m mm inch m mm inch m value mm value 30.0 207.0 0.305 11.5 79.3 0.500 0.0127 12.7 3.000 0.0762 76.2 10.000 0.254 254 8.650	Young's Modulus (E) [modulus of elasticity] Poisson's ratio (v) [transverse contraction 30.0 Modulus of elasticity (s) (psi x 10 ⁶) Wire Diameter [d] Spring Mean Diameter [D] Free Length [L ₁] Total coils [N ₁] Active coils [N ₂] (psi x 10 ⁶) (MPa x contraction 30.0 (psi x 10 ⁶) (MPa x 10 ³) inch m mm value value value 30.0 207.0 0.305 11.5 79.3 0.500 0.0127 12.7 3.000 0.0762 76.2 10.000 0.254 254 8.650 6.650

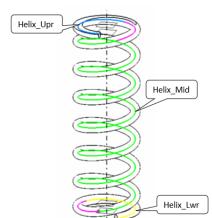
$$k = \frac{d^4G}{8D^3N_a}$$
 $v = \frac{E}{G \cdot 2} - 1$; $G = E / (2*(1+v))$

Calculated Pitch [P]				ring Outer meter [OD			ring Inner meter [ID]	Spring rate [k]			
inch	m	mm	inch	m	mm	inch	m	mm	lb/in	N/mm	
1.475	0.0375	37.475	3.500	0.0889	88.9	2.500	0.0635	63.5	500.45	87.64	

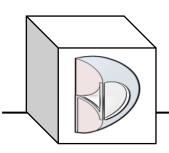
Spring Results (FEA)													
Mean Dia.	Force	defl	Rate										
mm	N	δ (mm)	(k) N/mm										
76.2	876.4	10	87.6										

in	lb	in	lb/in
3.000	197.03	0.394	500.4



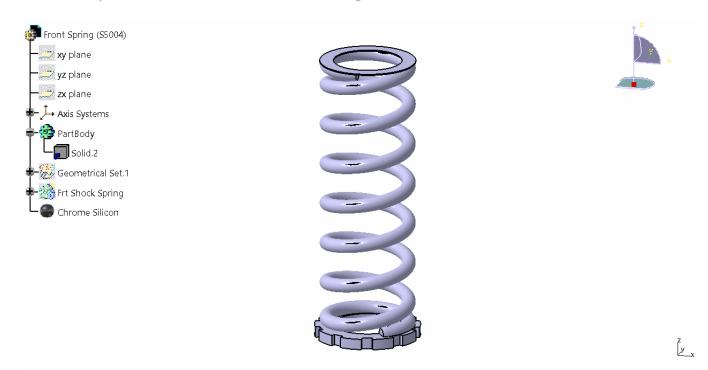


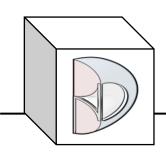
Adjusted for CATIA FEA
38.195 = Pitch in Helix_Mid
2.55 = Factor for Coils in Helix_Mid
6.10 = Coils in Helix_Mid
232.992 = Height in Helix_Mid
21.01 = Δ Free Length to Helix_Mid Ht.
10.504 = Height of Helix_Mid Start Plane
0.77 = Factor for Pitch in Helix_Upr&Lwr
0.50 = Factor for Height in Helix_Upr&Lwr
8.088 = Pitch in Helix_Upr&Lwr
5.252 = Height in Helix_Upr&Lwr





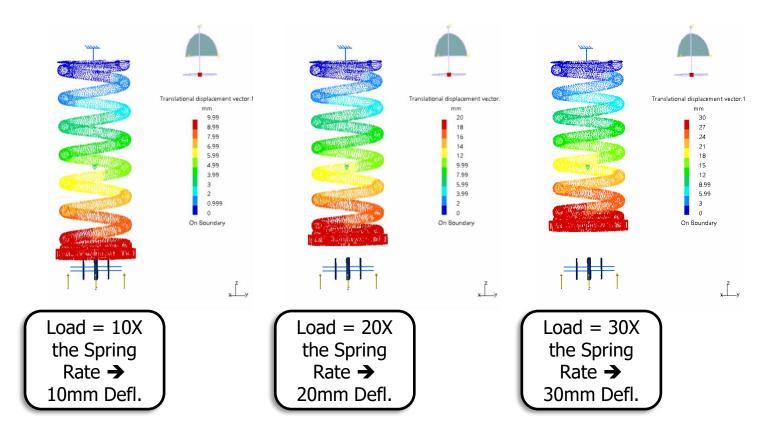
- 1.2) Create a CATIA Part model of the Spring.
 - Since this is an FEA simulation analysis of a coil over shock absorber assembly, we will assume the user has created all the parts within the assembly.

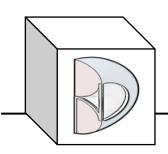






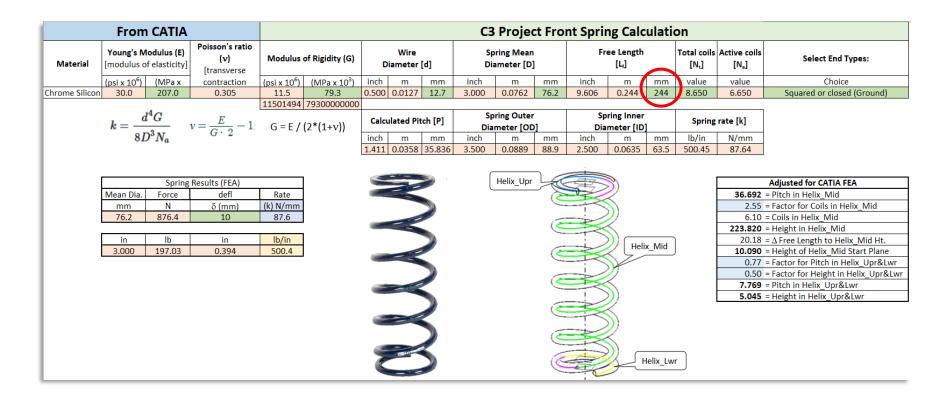
1.3) Create an FEA analysis of the Spring which correlates the Spring Rate of the CATIA Part model and proves the rate to be Linear.

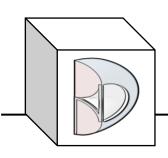






2.1) Change the Free Length of the Spring on the Calculation sheet to remove the deflection caused by the Preload value.

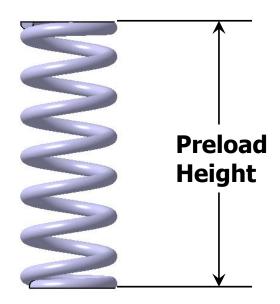


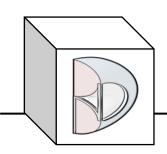




2.2) Update the CATIA Part for the Spring using the new values from the calculations sheet.

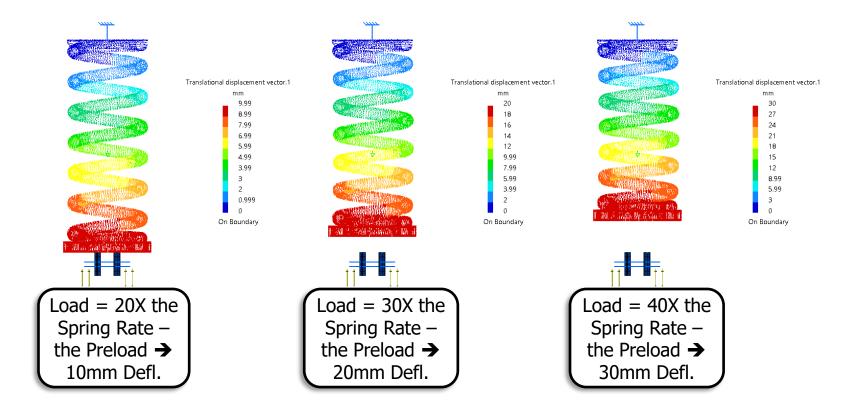
Adjusted for CATIA FEA
36.692 = Pitch in Helix_Mid
2.55 = Factor for Coils in Helix_Mid
6.10 = Coils in Helix_Mid
223.820 = Height in Helix_Mid
20.18 = ∆ Free Length to Helix_Mid Ht.
10.090 = Height of Helix_Mid Start Plane
0.77 = Factor for Pitch in Helix_Upr&Lwr
0.50 = Factor for Height in Helix_Upr&Lwr
7.769 = Pitch in Helix_Upr&Lwr
5.045 = Height in Helix_Upr&Lwr

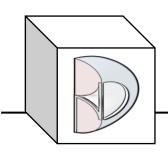






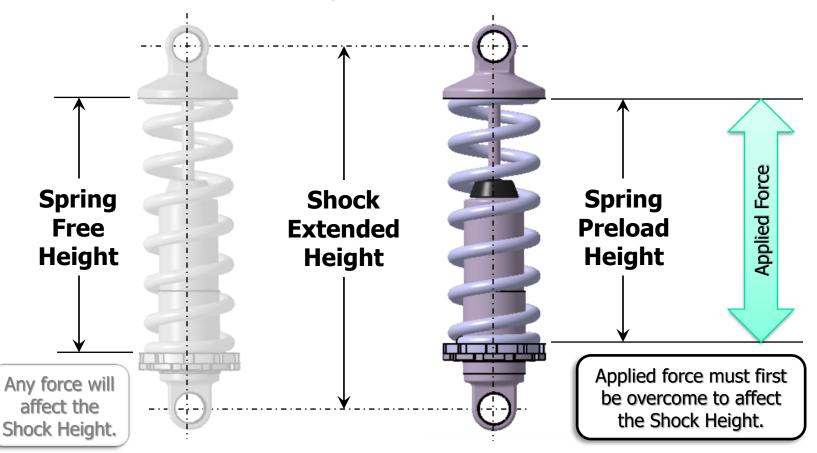
2.3) Create an FEA analysis of the <u>Preloaded</u> Spring to correlate the Spring Rate from the CATIA Part model and prove the rate remains Linear.

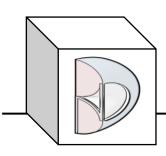






3.1) Create a CATIA Product model of the Coil Over Shock Absorber Assembly in the Preloaded condition.

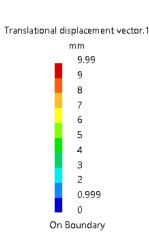




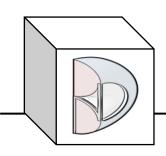


3.2) Create an FEA analysis (Static Case.Preload) of the Coil Over Assembly applying the proper restraints and loads. (10x rate = 10mm deflection)





Static Case.Preload will be used as the **Preload** for this simulation.



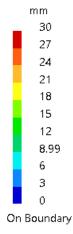


3.3) Create an FEA analysis (Static Case.Shock Load) of the Coil Over Assembly applying the proper restraints and loads.

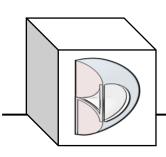
(30x rate = 30mm deflection)







Static Case. Shock Load will be used as the **Shock Load** for this simulation.

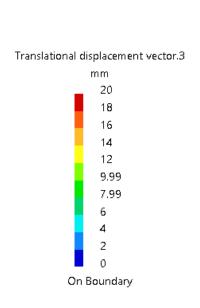




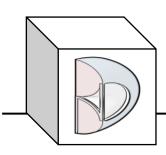
3.4) Create an FEA analysis (Combined Case.Shock Load) of the Coil Over Assembly applying the proper restraints and loads.

(Shock Load – Preload = Resultant Shock Load → Shock Deflection)



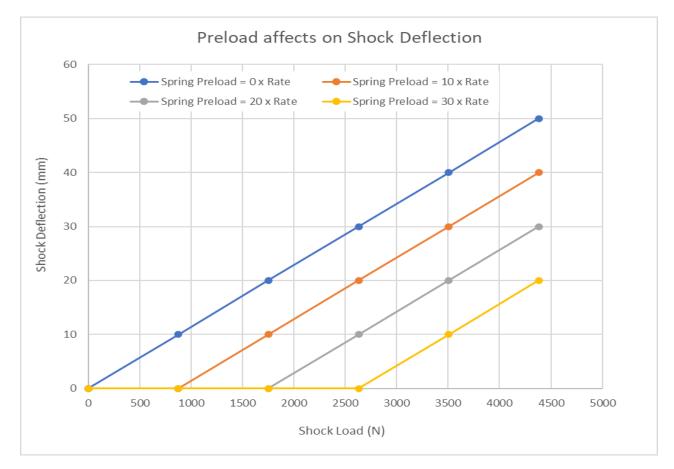


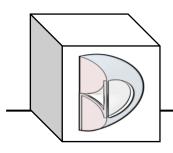
Combined Case.
Shock Load will be used as the
Resultant Shock
Load for this simulation.





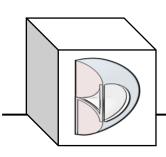
3.5) Graph below shows the Shock Deflection based on Shock Load at various Preload conditions.







Create the Free Length Spring FEA





Create an Excel spreadsheet to calculate the spring values.

	From CATIA				C3 Project Front Spring Calculation												
Material	Young's Modulus (E) Material [modulus of elasticity		Poisson's ratio (v) [transverse	Modulus of Rigidity (G)		Wire Diameter [d]		Spring Mean Diameter [D]			Free Length [L _f]			Total coils [N _t]	Active coils [N _a]	Select End Types:	
	(psi x 10 ⁶)	(MPa x	contraction	(psi x 10 ⁶)	$(MPa \times 10^3)$	inch	m	mm	inch	m	mm	inch	m	mm	value	value	Choice
Chrome Silico	n 30.0	207.0	0.305	11.5	79.3	0.500	0.0127	12.7	3.000	0.0762	76.2	10.000	0.254	254	8.650	6.650	Squared or closed (Ground)

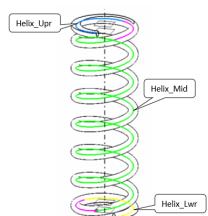
$$k = \frac{d^4G}{8D^3N_a}$$
 $v = \frac{E}{G \cdot 2} - 1$ $G = E / (2*(1+v))$

Calcu	ılated Pit	ch [P]		ring Outer meter [OD			ring Inner meter [ID]	Spring rate [k]			
nch	m	mm	inch	m	mm	inch	m	mm	lb/in	N/mm	
.475	0.0375	37.475	3.500	0.0889	88.9	2.500	0.0635	63.5	500.45	87.64	

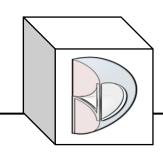
	Spring Results (FEA)													
Mean Dia.	Force	defl	Rate											
mm	N	δ (mm)	(k) N/mm											
76.2	876.4	10	87.6											
	_		_											

in	lb	in	lb/in
3.000	197.03	0.394	500.4



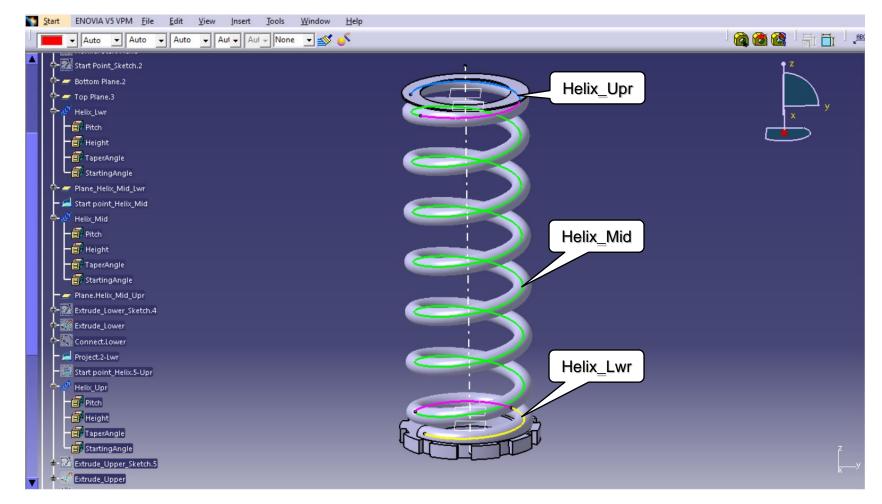


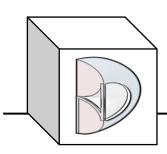
	Adjusted for CATIA FEA
38.195	= Pitch in Helix_Mid
2.55	= Factor for Coils in Helix_Mid
6.10	= Coils in Helix_Mid
232.992	= Height in Helix_Mid
21.01	= Δ Free Length to Helix_Mid Ht.
10.504	= Height of Helix_Mid Start Plane
0.77	= Factor for Pitch in Helix_Upr&Lwr
0.50	= Factor for Height in Helix_Upr&Lwr
8.088	= Pitch in Helix_Upr&Lwr
5.252	= Height in Helix_Upr&Lwr





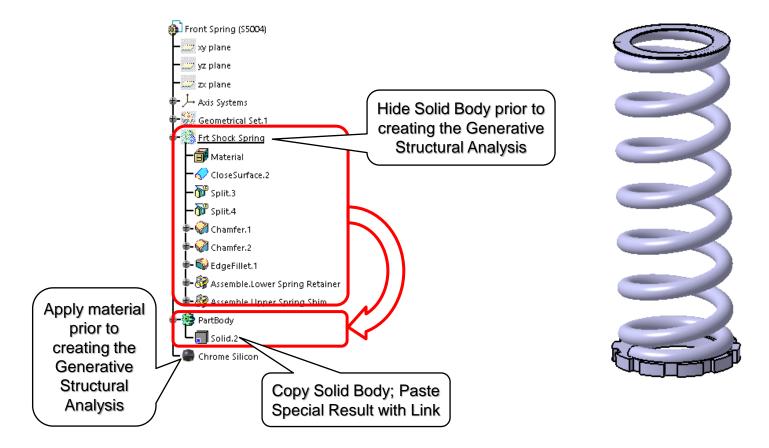
Create the Spring based on calculated the spring values.

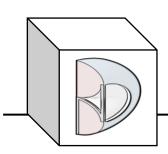






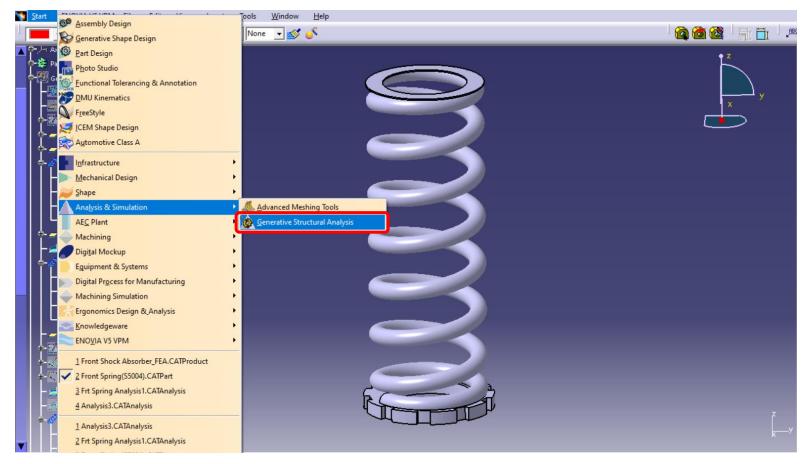
Generative Structural Analysis only works with the geometry inside the <u>PartBody!</u>

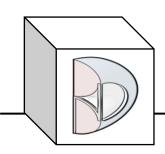






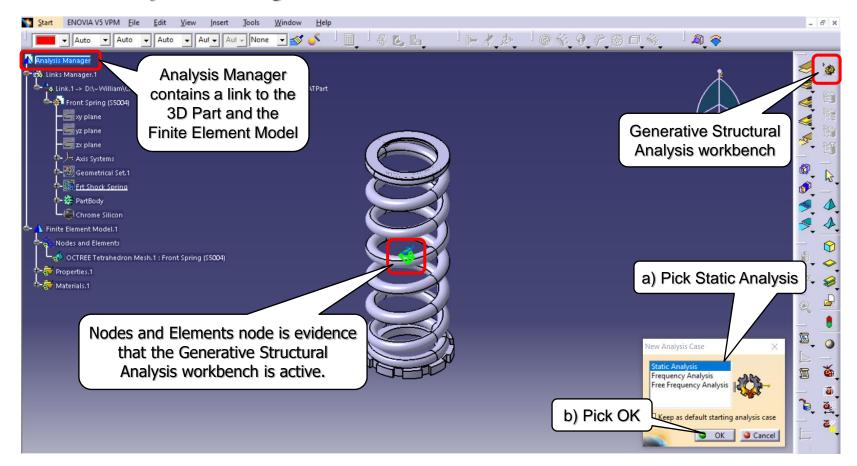
While inside the CatPart, call the Generative Structural Analysis workbench.

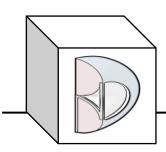






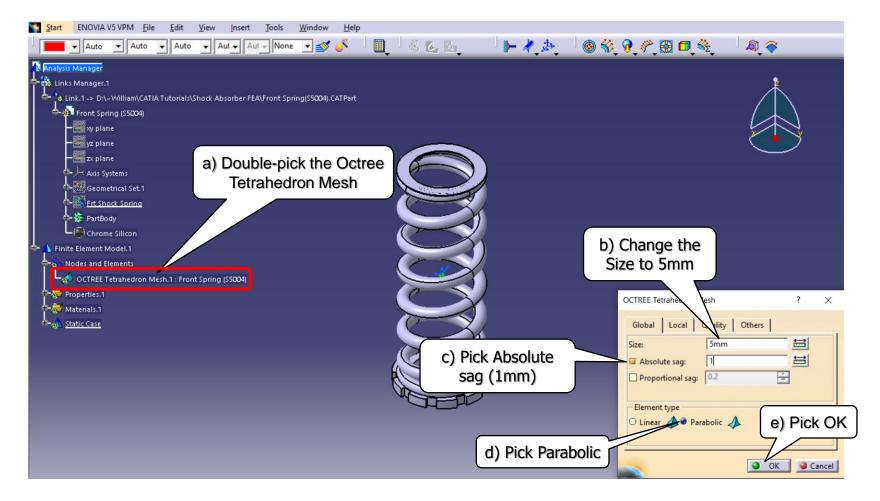
 Generative Structural Analysis workbench creates the Analysis Manager.

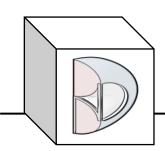






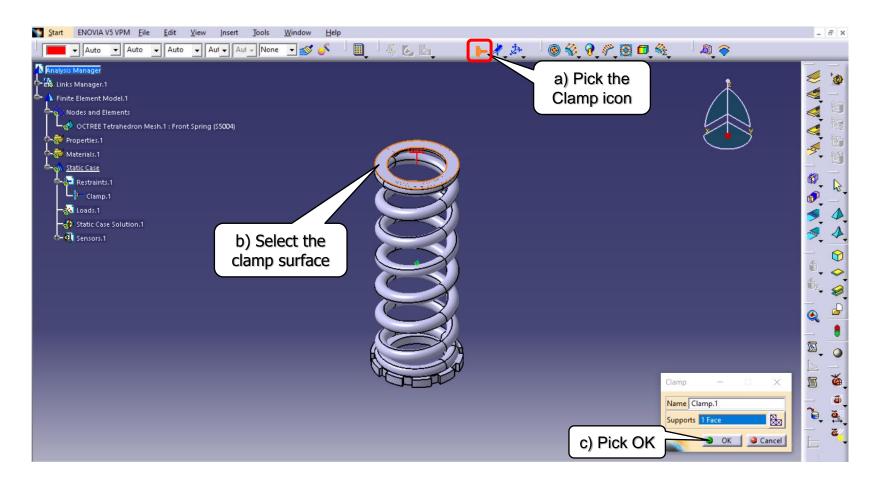
Optimize the Mesh for the Spring.

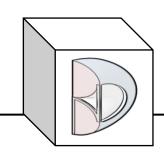






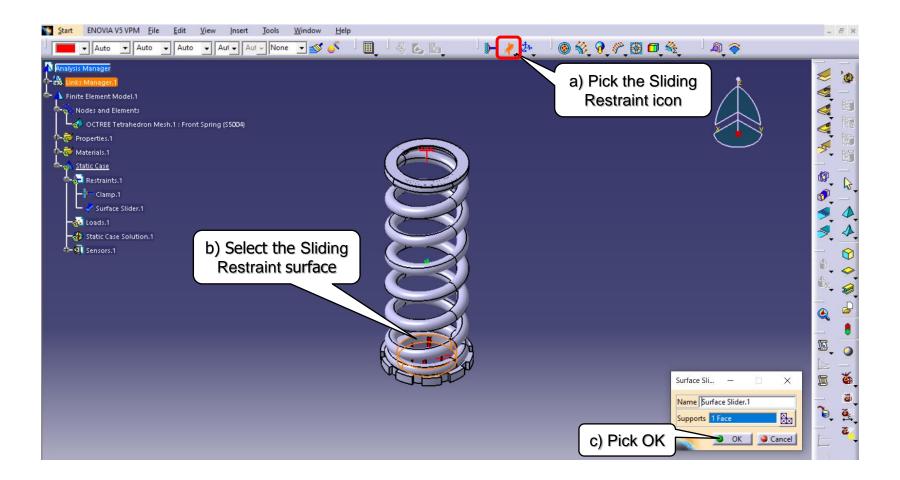
Create the Clamp Restraint.

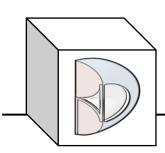






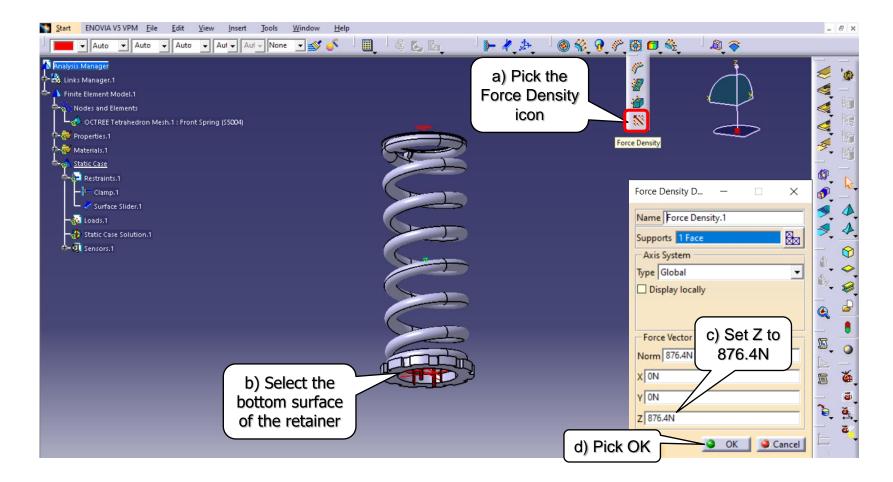
Create the Sliding Restraint.

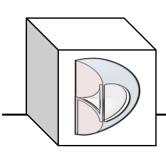






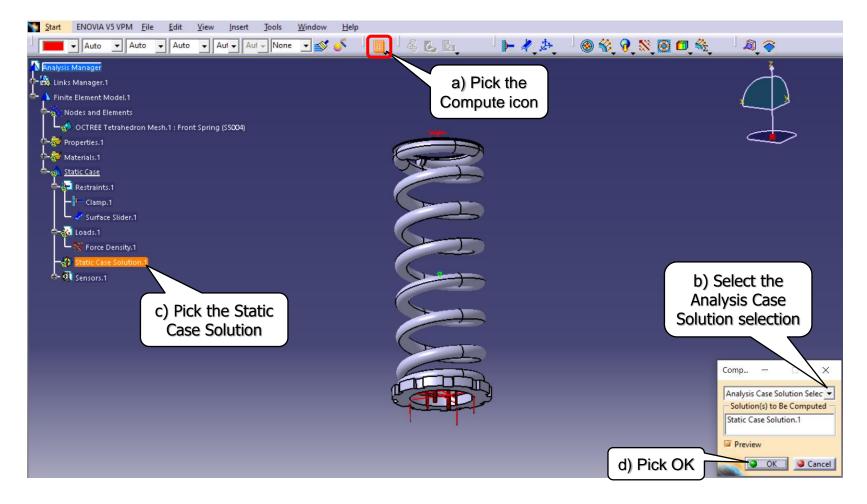
Create the Load (10 x rate → 876.4N).

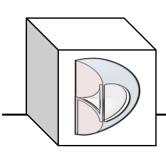






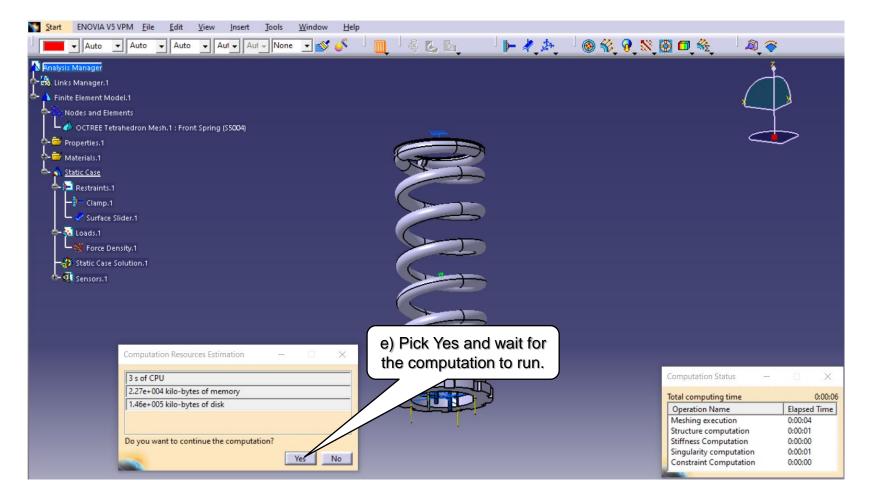
Compute the analysis of the Free Length Spring.

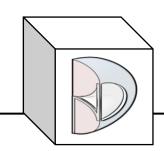






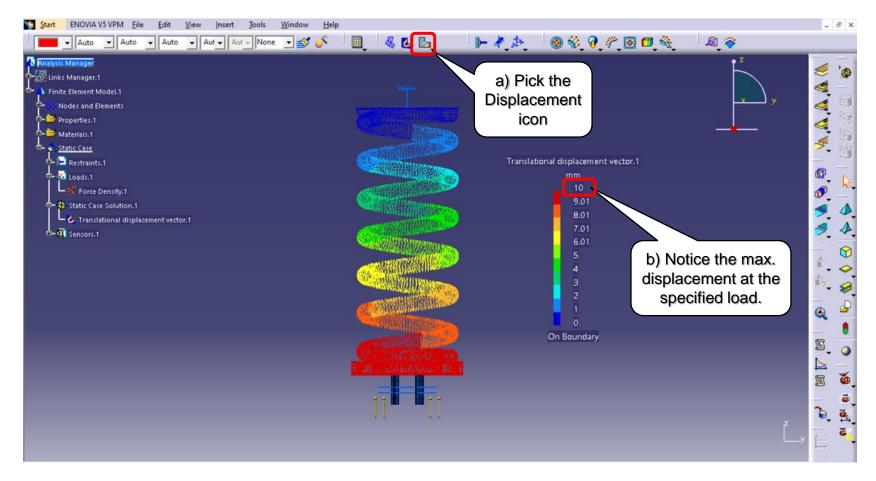
Compute the analysis of the Free Length Spring.

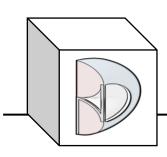






Show results of the analysis.







Adjust Factors to "dial in" the FEA correlation if required.

	From CATIA				C3 Project Front Spring Calculation												
Material	Young's Modulus (E) Material [modulus of elasticity		Poisson's ratio (v) [transverse	Modulus of Rigidity (G)		Wire Diameter [d]		Spring Mean Diameter [D]			Free Length [4]			Total coils [N _t]	Active coils [N _a]	Select End Types:	
	(psi x 10 ⁶)	(MPa x	contraction	(psi x 10 ⁶)	$(MPa \times 10^3)$	inch	m	mm	inch	m	mm	inch	m	mm	value	value	Choice
Chrome Silico	n 30.0	207.0	0.305	11.5	79.3	0.500	0.0127	12.7	3.000	0.0762	76.2	10.000	0.254	254	8.650	6.650	Squared or closed (Ground)

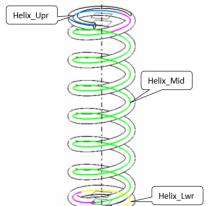
$$k = \frac{d^4G}{8D^3N_a}$$
 $v = \frac{E}{G \cdot 2} - 1$ $G = E / (2*(1+v))$

Calculated Pitch [P]				ring Outer meter [OD			ring Inner meter [ID]	Spring rate [k]		
inch	m	mm	inch	m	mm	inch	m	mm	lb/in	N/mm
.475	0.0375	37.475	3.500	0.0889	88.9	2.500	0.0635	63.5	500.45	87.64

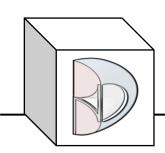
Spring Results (FEA)											
Mean Dia.	Force	defl	Rate								
mm	N	δ (mm)	(k) N/mm								
76.2	876.4	10	87.6								

in	lb	in	lb/in
3.000	197.03	0.394	500.4



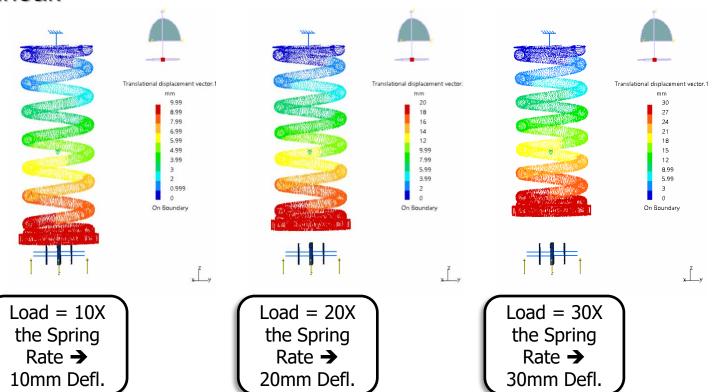


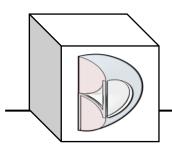
Adjusted for CATIA FEA
38.195 = Pitch in Helix Mid
2.55 = Factor for Coils in Helix_Mid
6.10 = Coils in Helix_Mid
232.992 = Height in Helix_Mid
21.01 = ∆ Free Length to Helix_Mid Ht.
10.504 = Height of Helix Mid Start Plane
0.77 = Factor for Pitch in Helix_Upr&Lwr
0.50 = Factor for Height in Helix Upr&Lwr
8.088 = Pitch in Helix_Upr&Lwr
5.252 = Height in Helix_Upr&Lwr





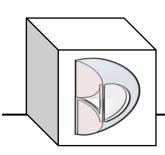
 The FEA analysis of the Free Length Spring correlates with the Spring Rate of the CATIA Part model and proves the rate to be Linear.





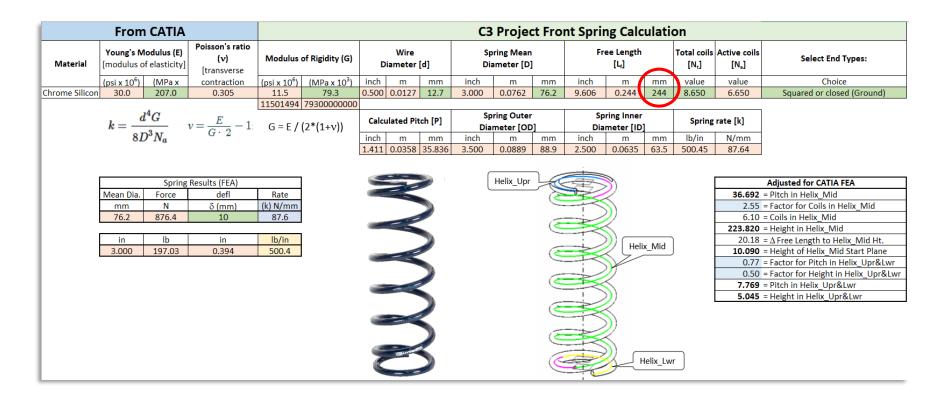


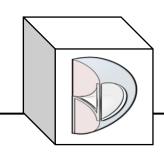
Create the Preload Length Spring FEA





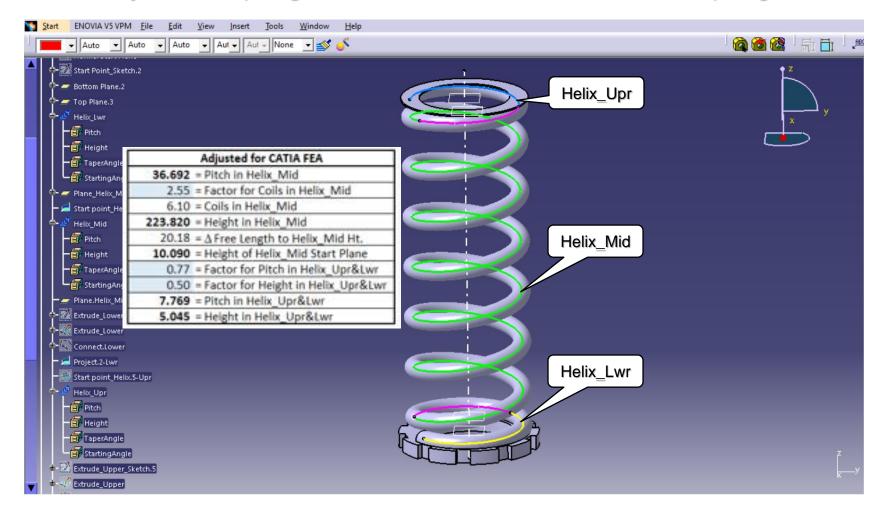
 Change the Free Length of the Spring on the Calculation sheet to remove the deflection caused by the Preload value.

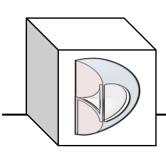






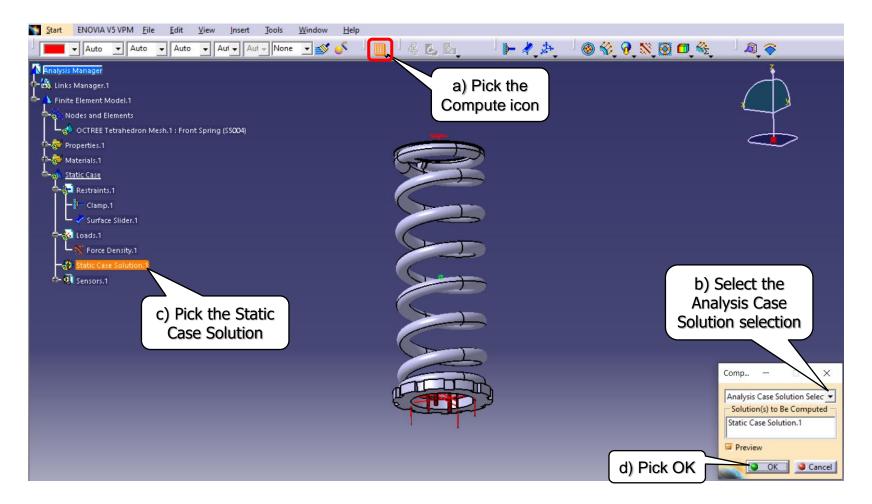
Adjust the Spring based on Preload calculated the spring values.

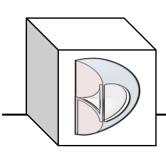






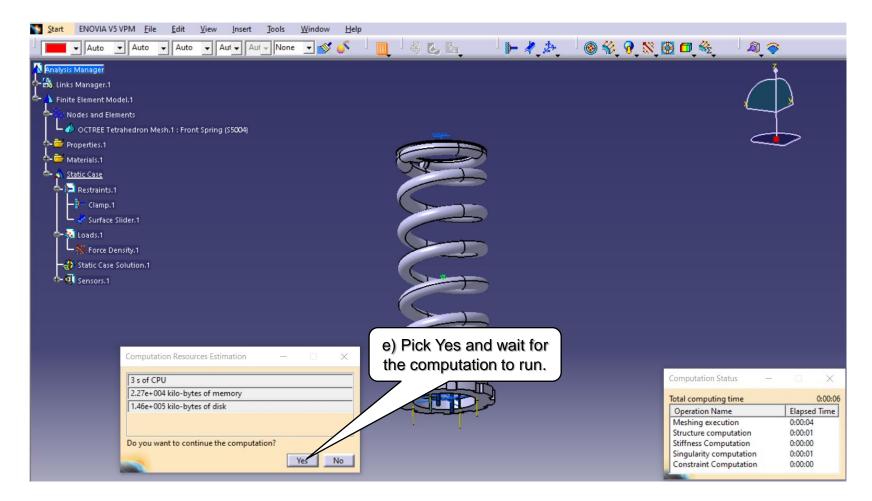
Compute the analysis of the Preloaded Spring.

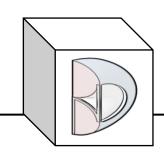






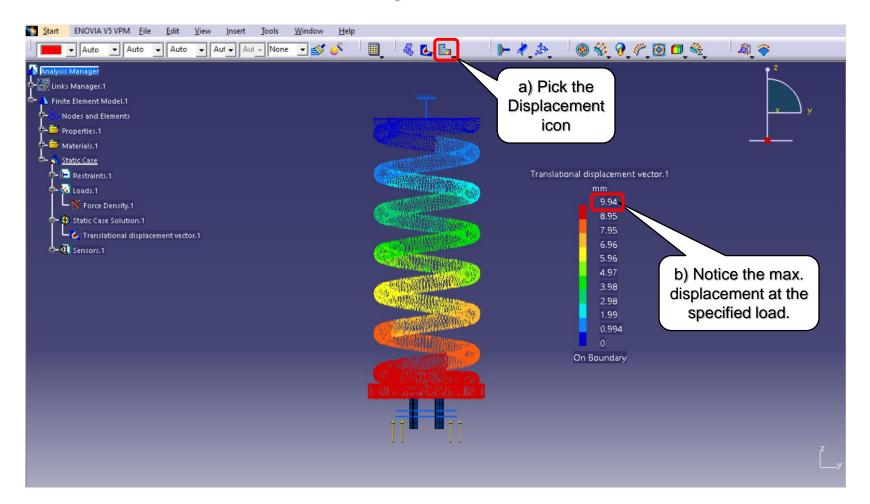
Compute the analysis of the Preloaded Spring.

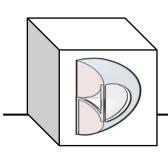






Show results of the analysis.







Adjust Factors to "dial in" the FEA correlation if required.

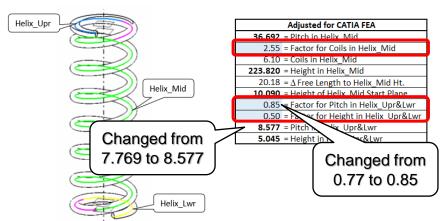
	From		C3 Project Front Spring Calculation														
Young's Modulus (E) Material [modulus of elasticity]		(v)		Modulus of Rigidity (G) Wire Diameter [d]		Spring Mean Diameter [D]		Free Length [4]		Total coils [N _t]	Active coils [N _a]	Select End Types:					
	(psi x 10 ⁶)	(MPa x	contraction	(psi x 10 ⁶)	(MPa x 10 ³)	inch	m	mm	inch	m	mm	inch	m	mm	value	value	Choice
Chrome Silicon	30.0	207.0	0.305	11.5	79.3	0.500	0.0127	12.7	3.000	0.0762	76.2	9.606	0.244	244	8.650	6.650	Squared or closed (Ground)

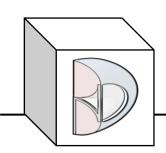
$$k = \frac{d^4G}{8D^3N_a}$$
 $v = \frac{E}{G \cdot 2} - 1$ $G = E / (2*(1+v))$

Calculated Pitch [P]			•	ring Outer meter [OD			ring Inner meter [ID]	Spring rate [k]		
inch	m	mm	inch	m	mm	inch	m	mm	lb/in	N/mm
L.411	0.0358	35.836	3.500	0.0889	88.9	2.500	0.0635	63.5	500.45	87.64

Spring Results (FEA)											
Mean Dia.	Force	defl	Rate								
mm	N	δ (mm)	(k) N/mm								
76.2	876.4	10	87.6								
in	lb	in	lb/in								
3.000	197.03	0.394	500.4								

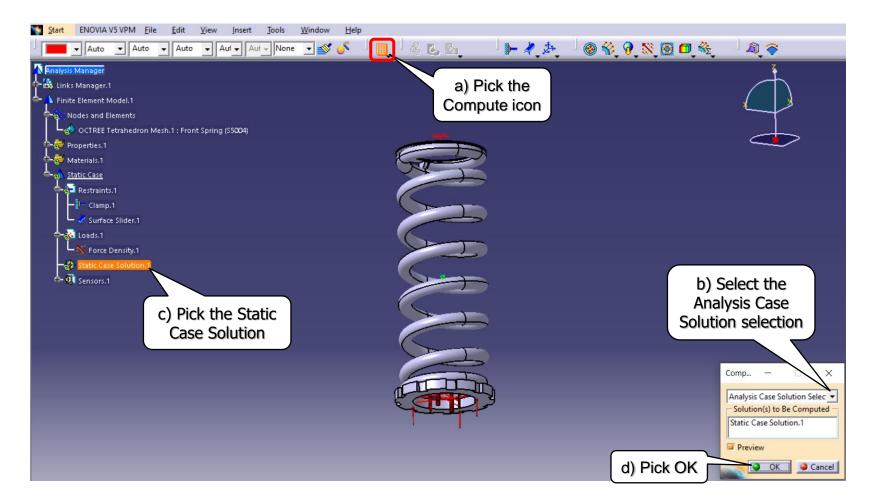


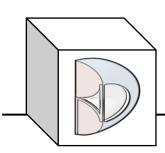






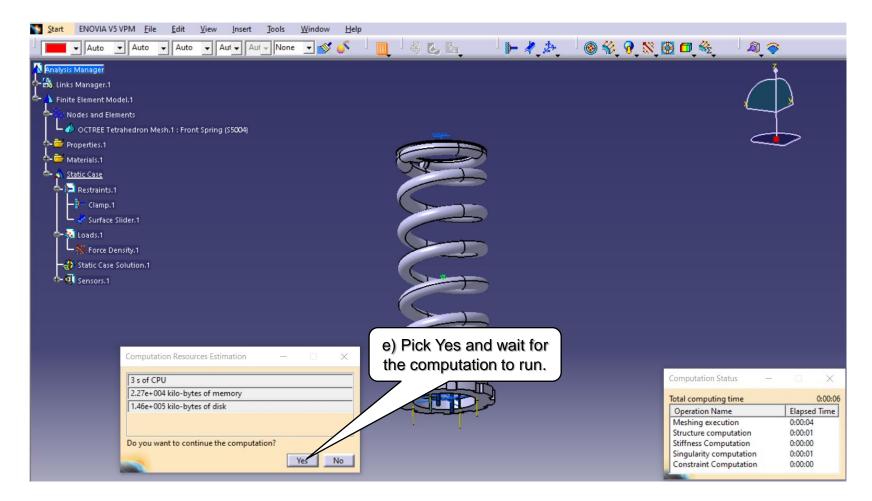
Re-compute the analysis of the Preloaded Spring.

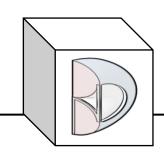






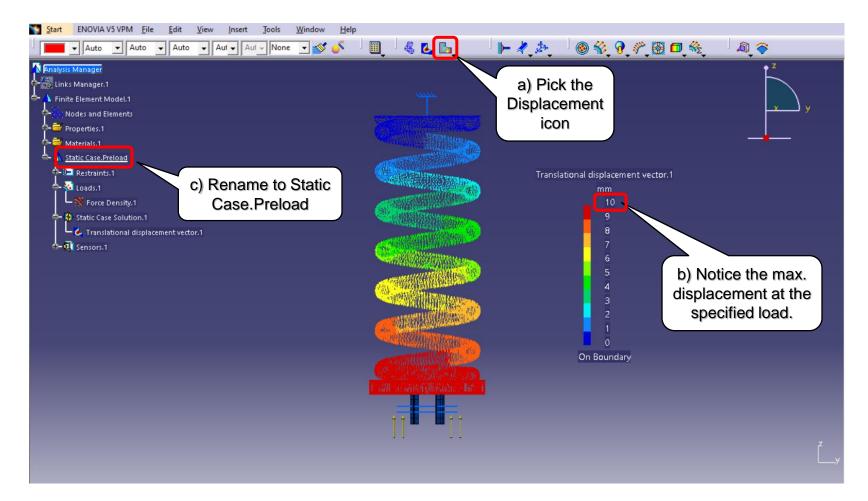
Re-compute the analysis of the Preloaded Spring.

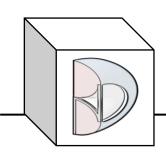






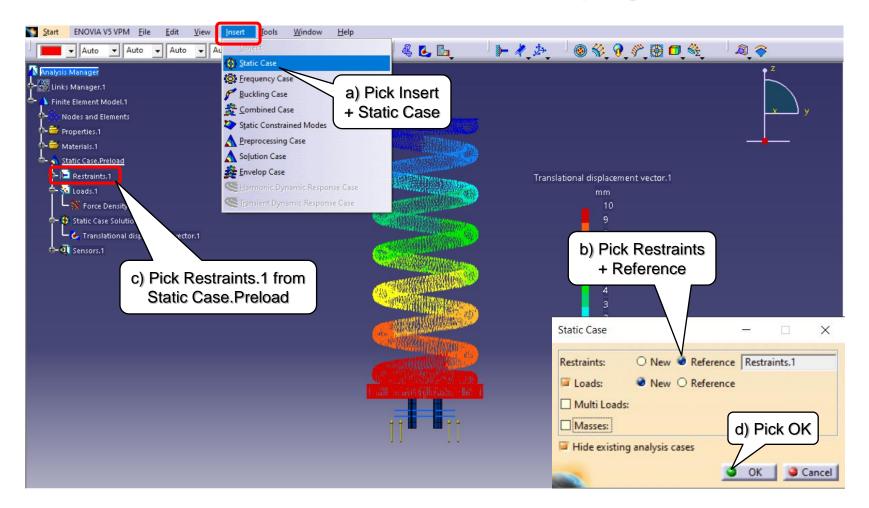
Show results of the Preload analysis.

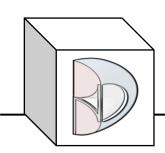






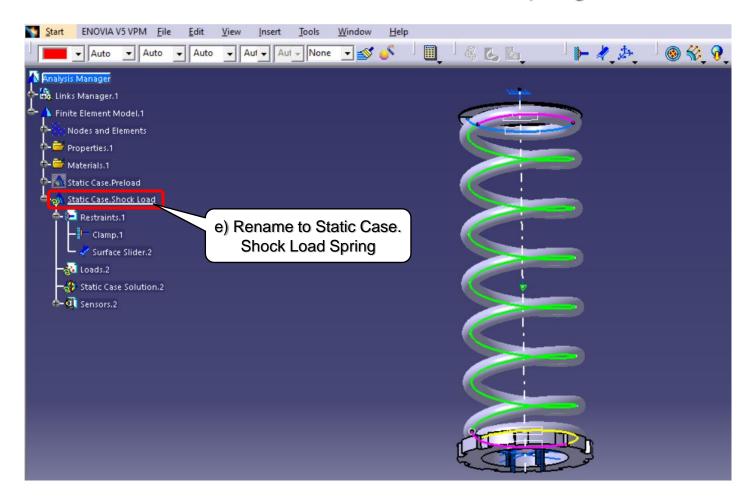
Create a new Static Case.Shock Load Spring.

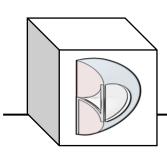






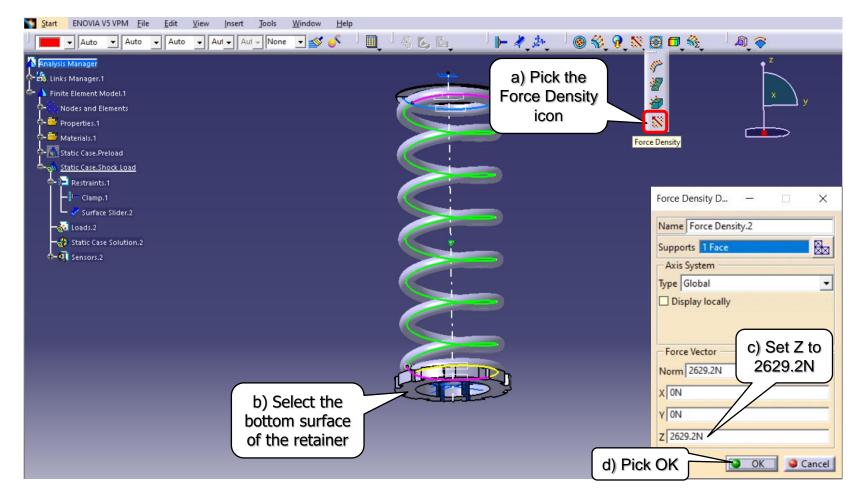
Create a new Static Case.Shock Load Spring.

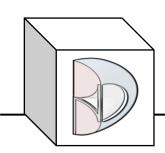






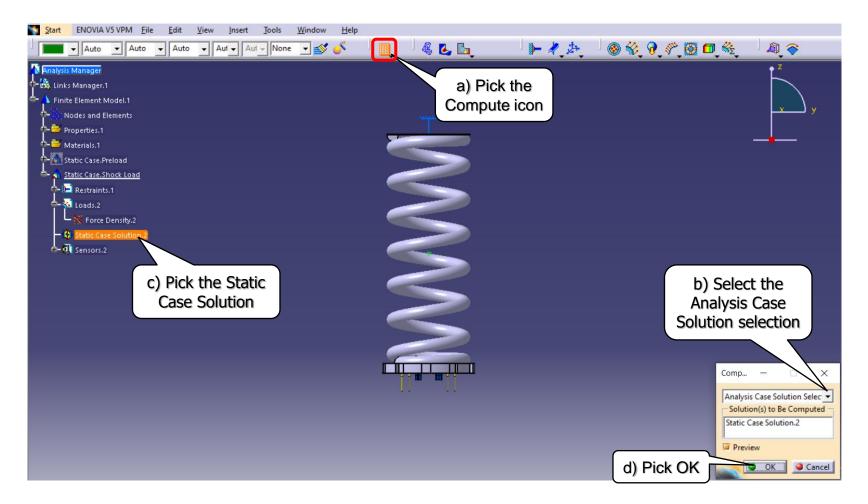
Create the new Shock Spring Load (30 x rate → 2629.2N).

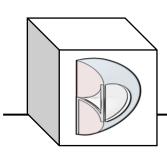






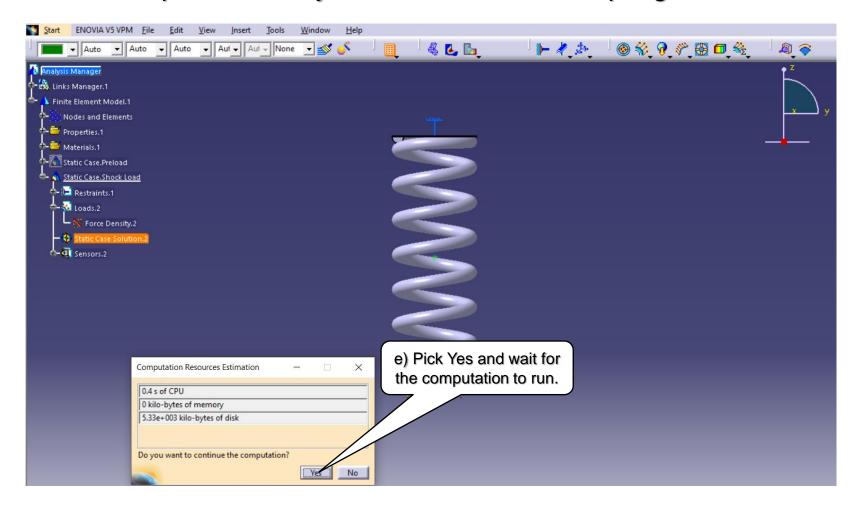
Compute the analysis of the Shock Load Spring.

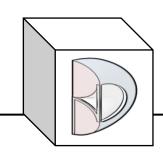






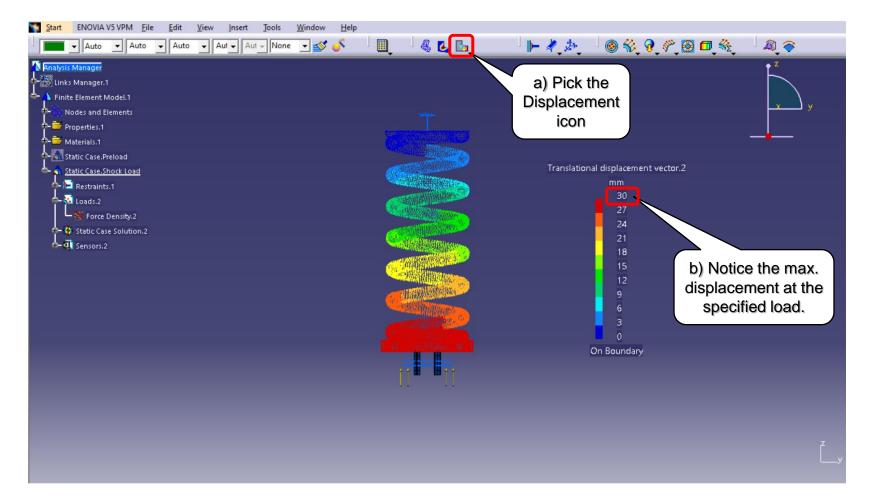
Compute the analysis of the Shock Load Spring.

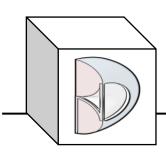






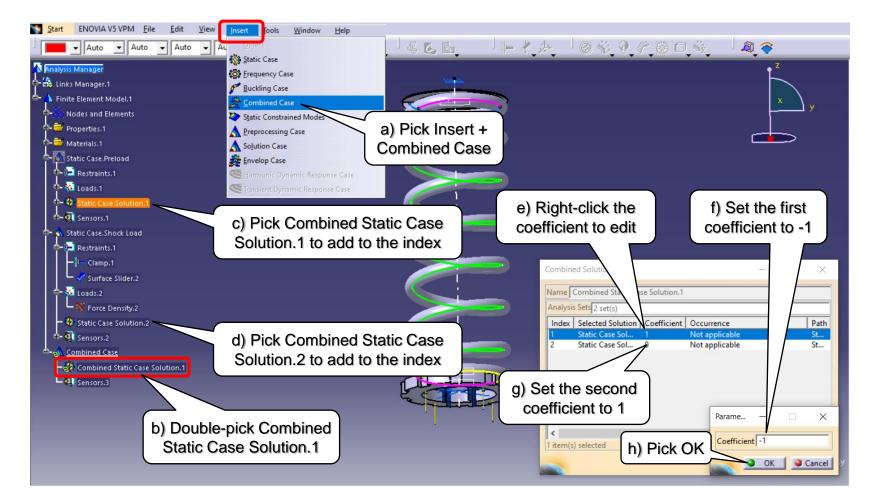
Show results of the Shock Load Spring analysis.

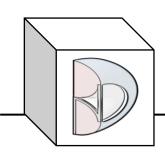






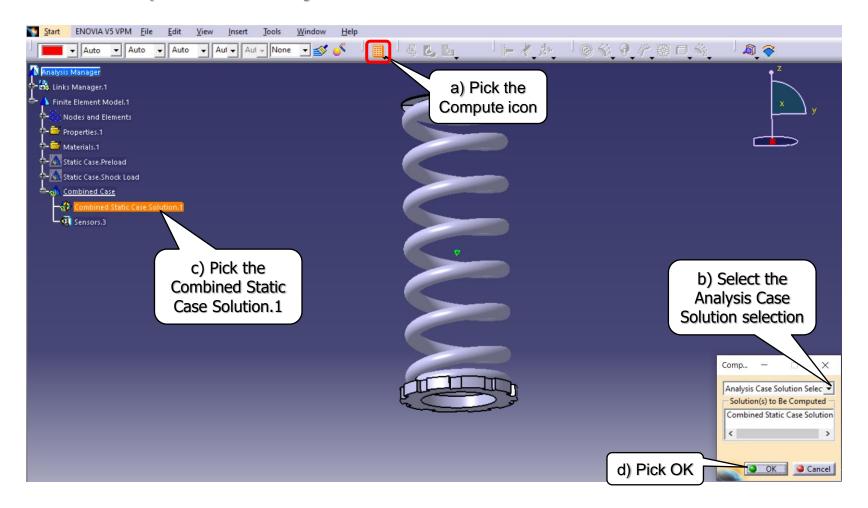
Create a new Combined Case.Shock Spring Deflection.

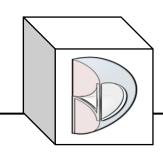






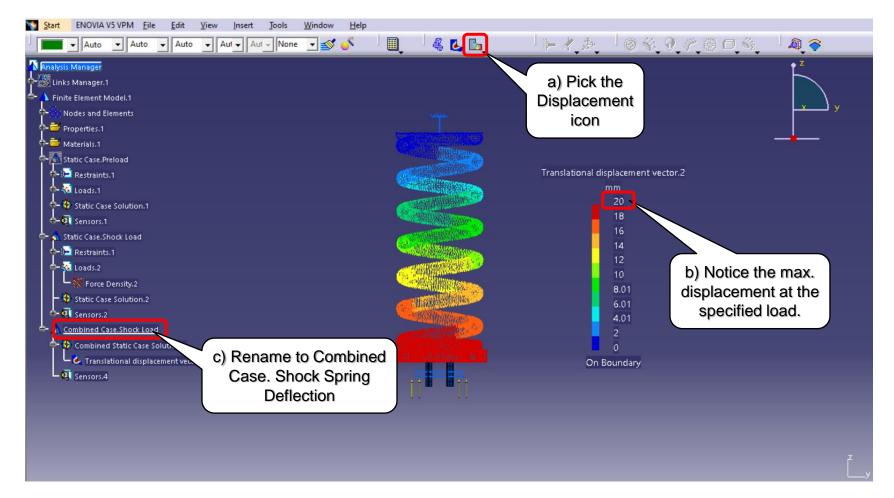
Compute the analysis of the Combined Static Case Solution.1

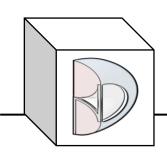






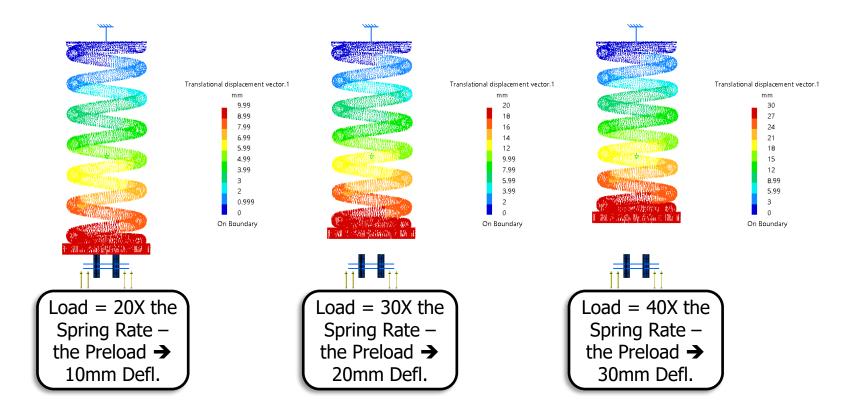
Show analysis results of the Combined Case. Shock Spring Deflection.

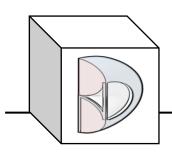






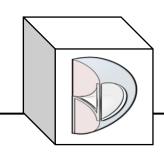
 The FEA analysis of the <u>Preloaded</u> Spring correlates with the Spring Rate from the CATIA Part model and proves the rate remains Linear.





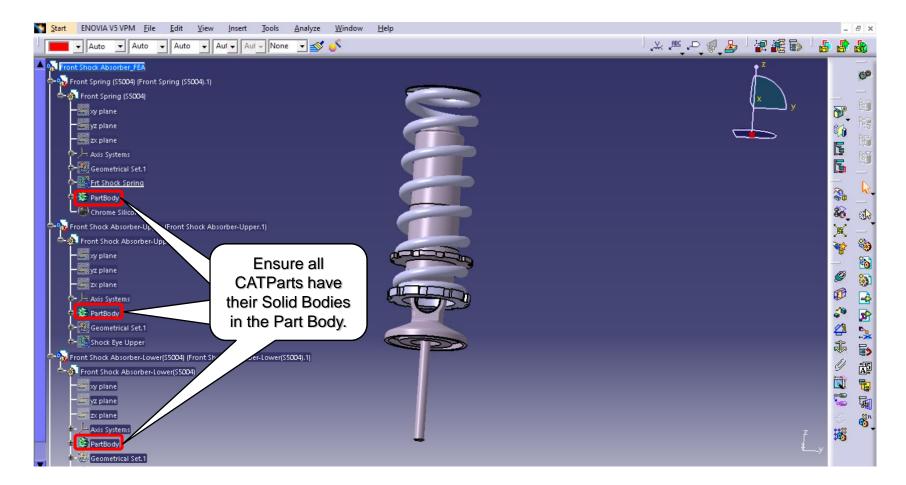


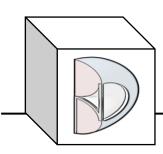
Create the Preloaded Coil-over Shock Assembly FEA





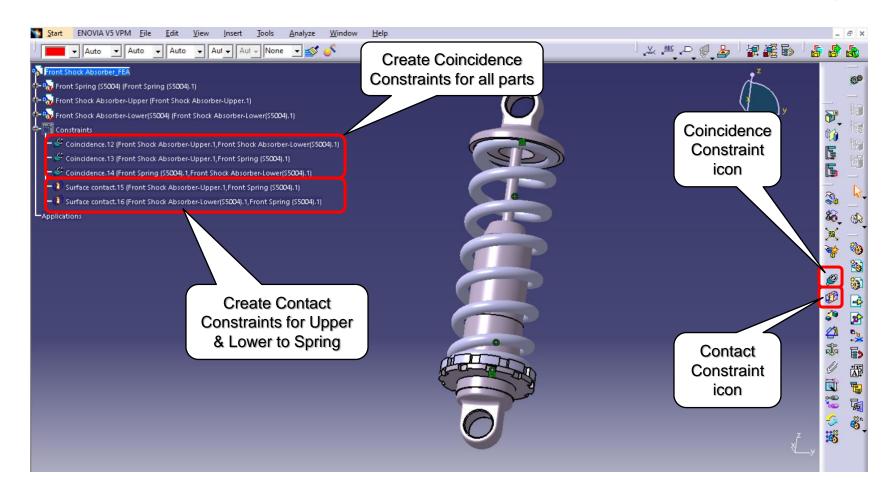
Create a CATProduct for the Coil-over Shock Assy.

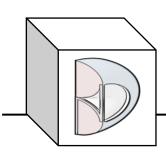






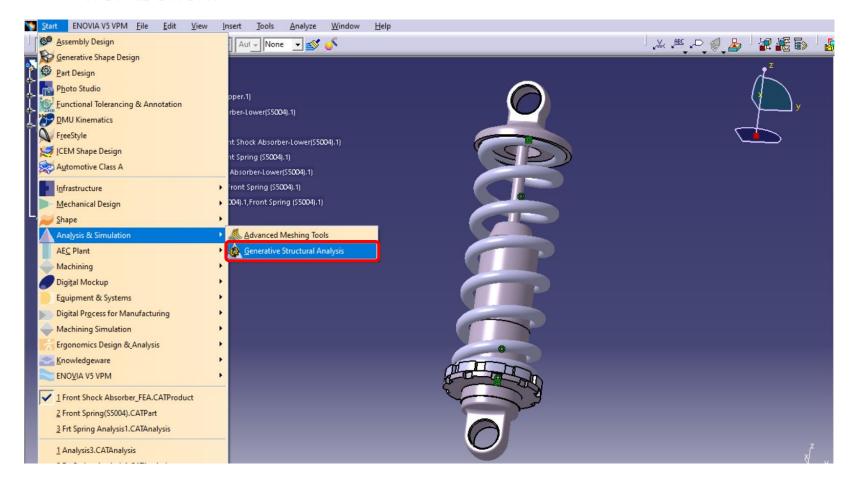
Create Constraints for all parts within the Coil-over Shock Assy.

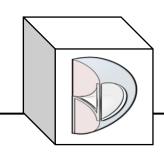






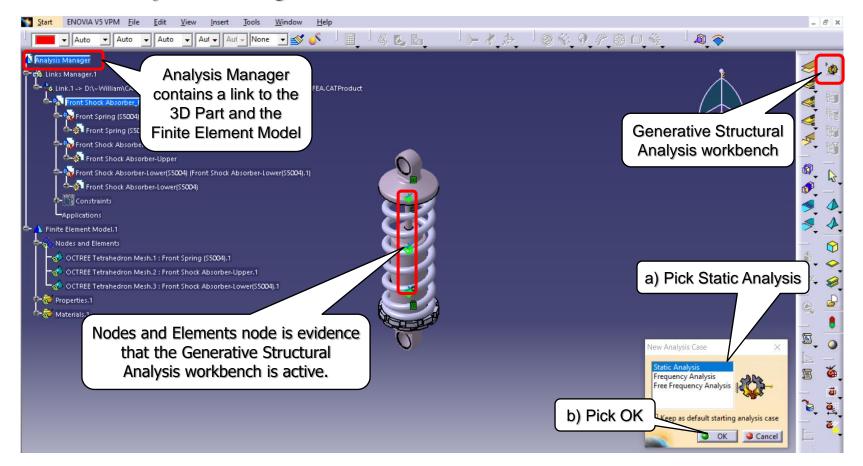
While inside the CatPart, call the Generative Structural Analysis workbench.

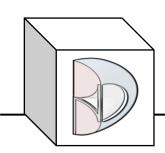






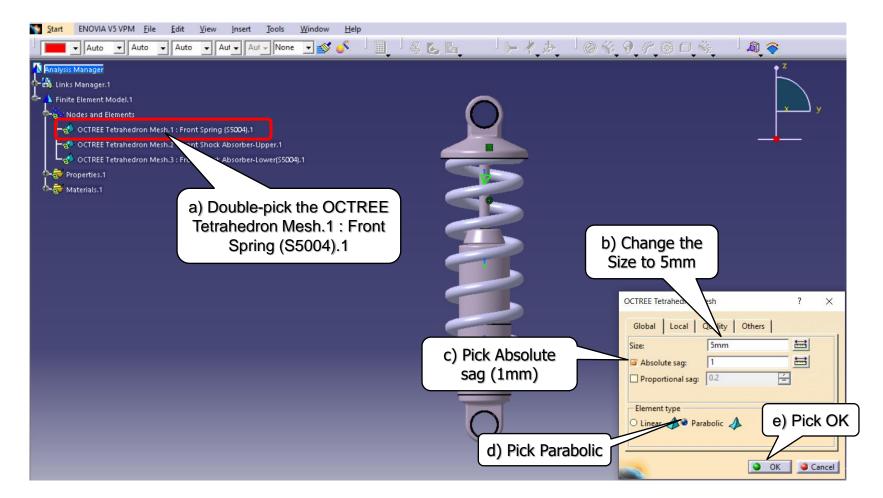
 Generative Structural Analysis workbench creates the Analysis Manager.

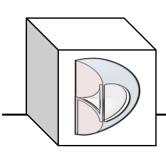






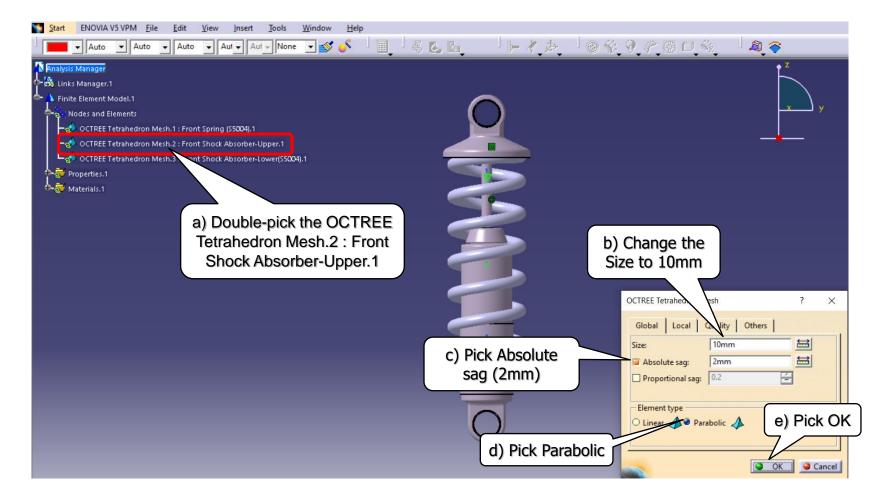
Optimize the Mesh for the Spring.

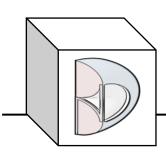






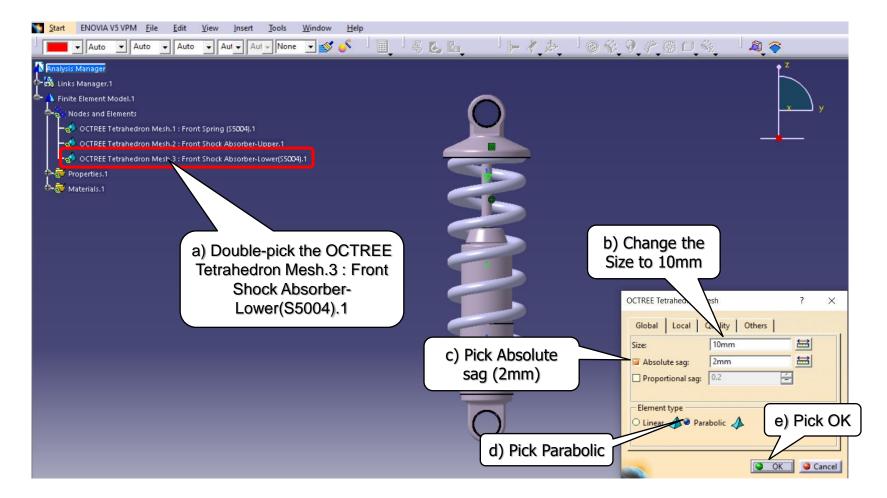
Optimize the Mesh for the Upper Shock.

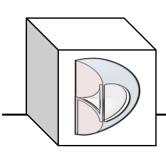






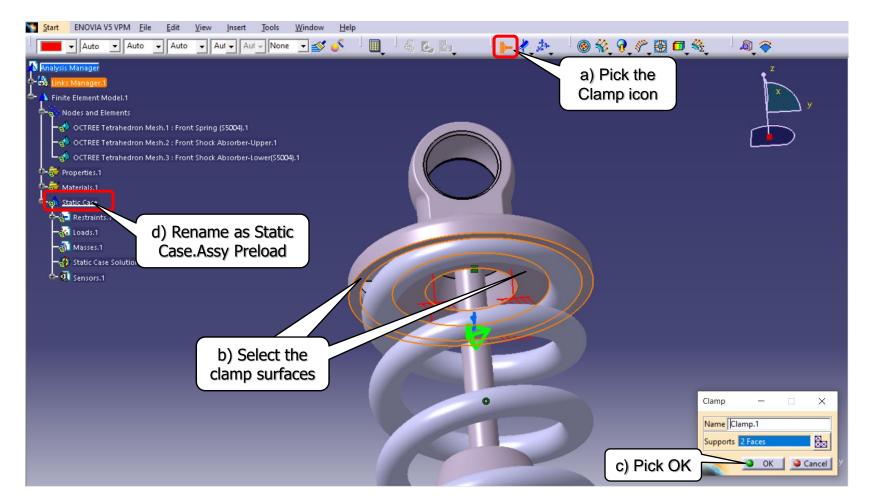
Optimize the Mesh for the Lower Shock.

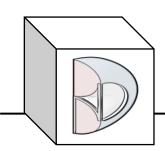






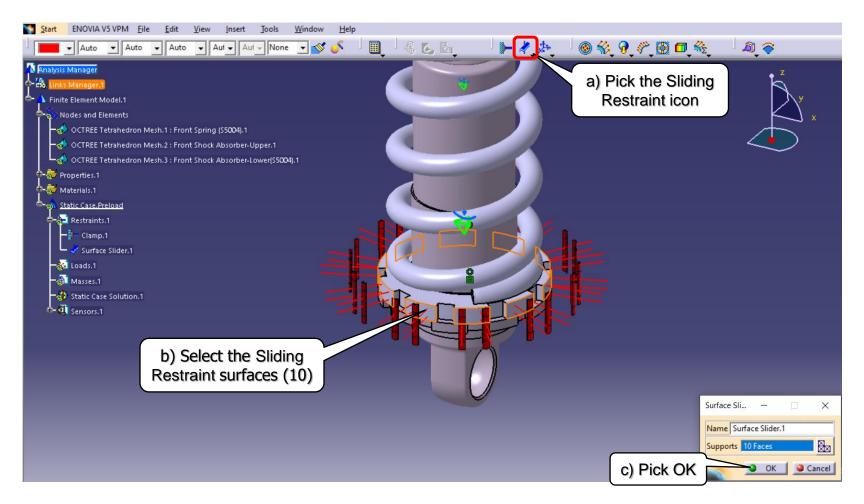
Create the Clamp Restraint and rename Static Case.

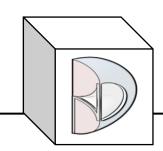






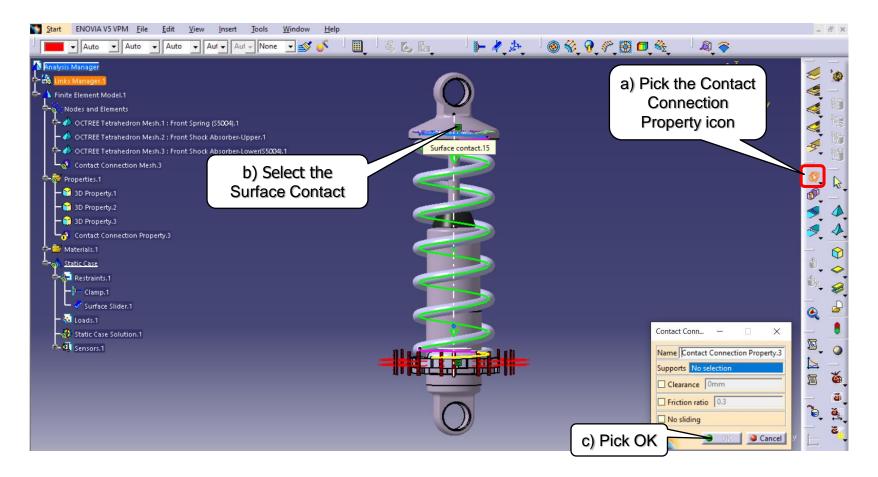
Create the Sliding Restraint.

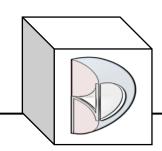






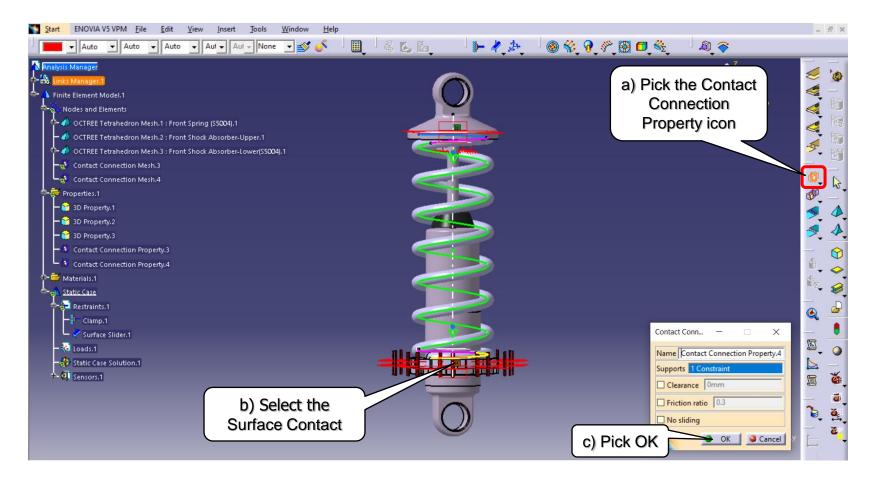
Create the Contact Connection Property.1

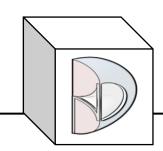






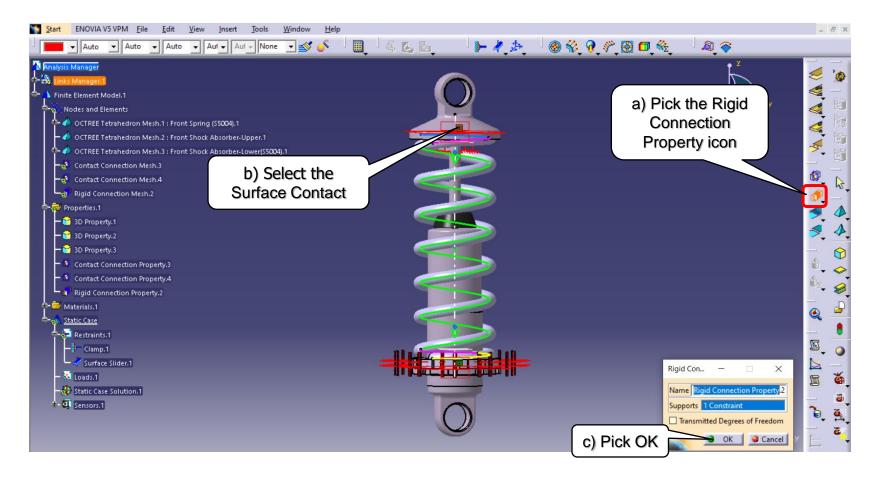
Create the Contact Connection Property.2

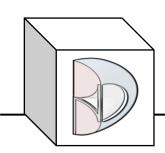






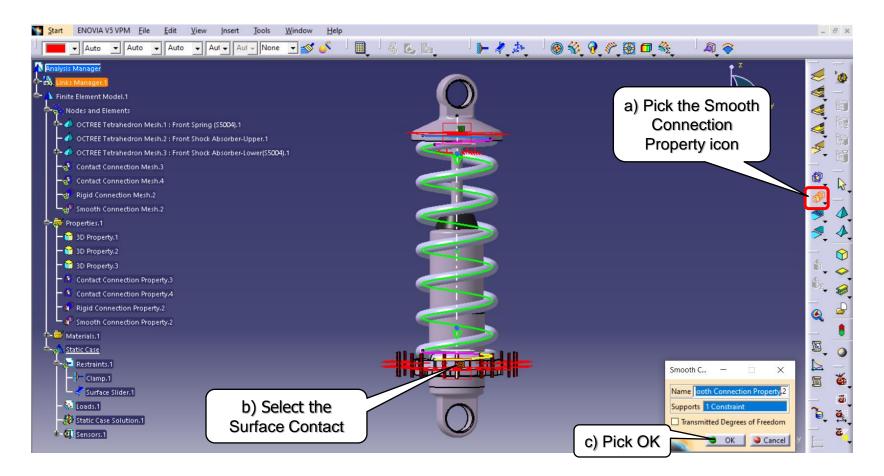
Create the Rigid Connection Property.

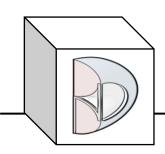






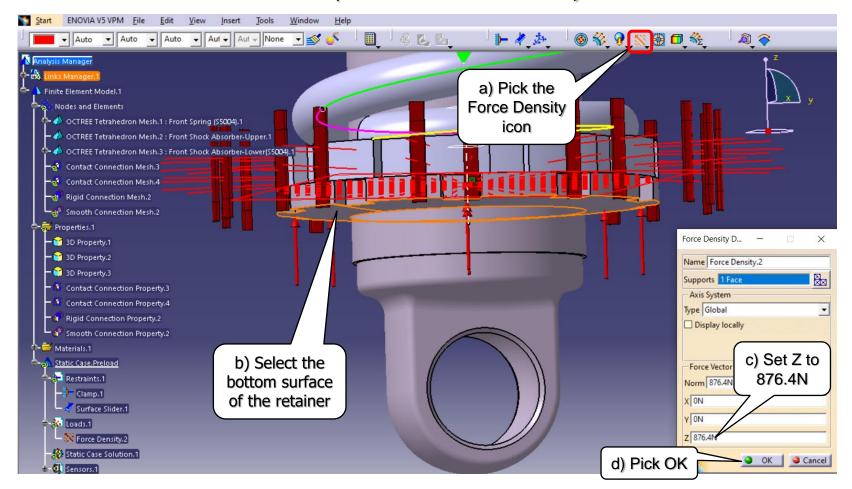
Create the Smooth Connection Property.

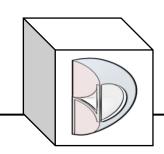






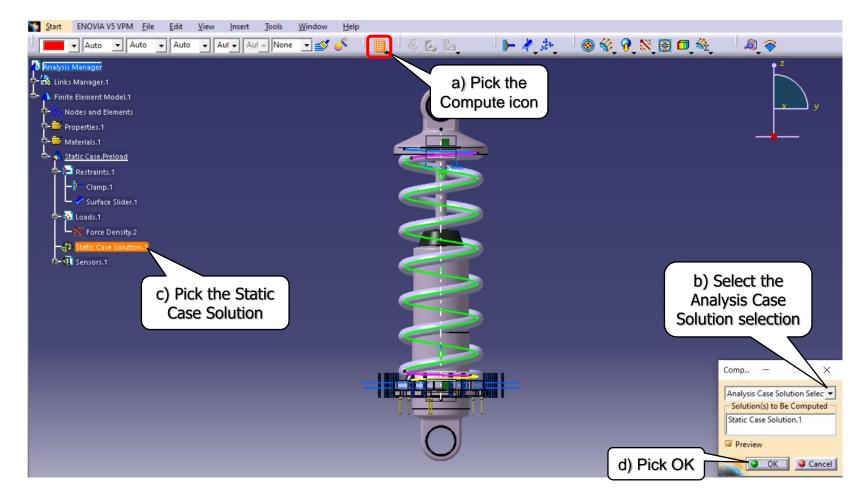
Create the Preload (10 x rate → 876.4N).

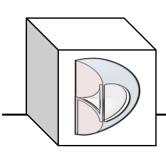






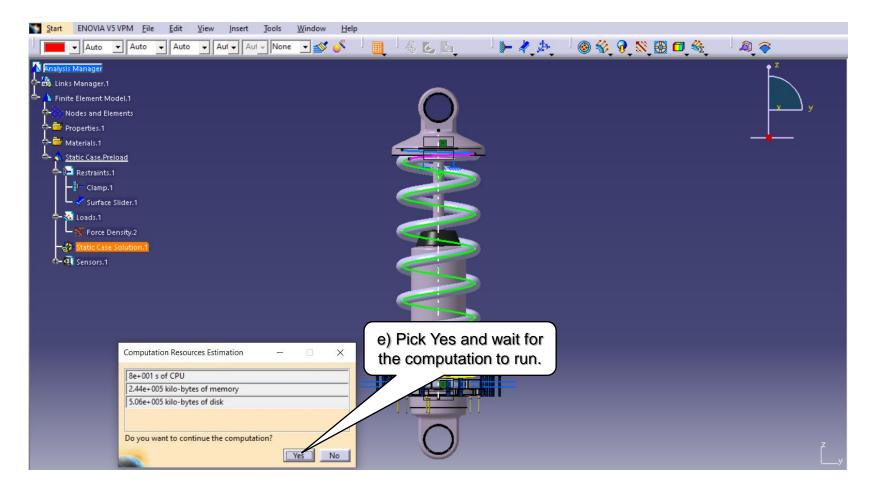
Compute the Assy Preload analysis.

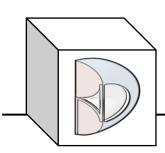






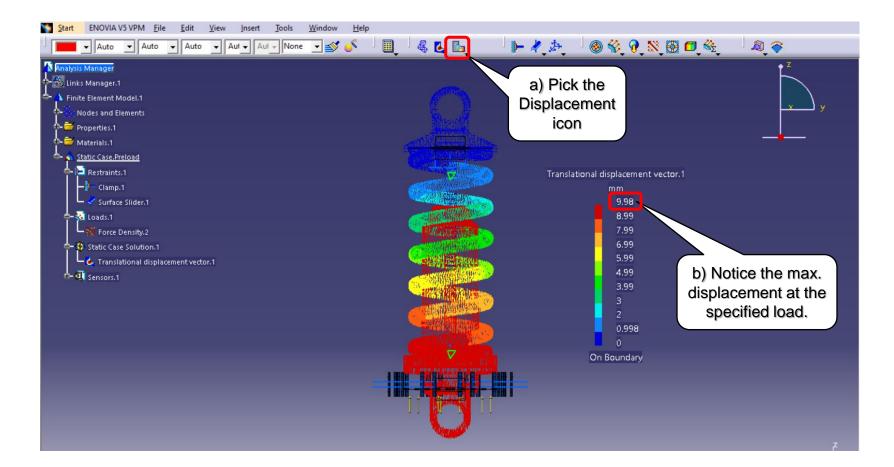
Compute the Assy Preload analysis.

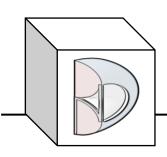






Show results of the Assy Preload analysis.







Adjust Factors to "dial in" the FEA correlation if required.

From CATIA				C3 Project Front Spring Calculation													
Material	Young's Modulus (E) [modulus of elasticity]		Poisson's ratio (v) [transverse	Modulus of Rigidity (G)		Wire Diameter [d]		Spring Mean Diameter [D]		Free Length [L _r]		Total coils Active coils [N _t]		Select End Types:			
	(psi x 10 ⁶)	(MPa x	contraction	(psi x 10 ⁶)	(MPa x 10 ³)	inch	m	mm	inch	m	mm	inch	m	mm	value	value	Choice
Chrome Silicon	30.0	207.0	0.305	11.5	79.3	0.500	0.0127	12.7	3.000	0.0762	76.2	9.606	0.244	244	8.650	6.650	Squared or closed (Ground)
				11501494	79300000000												

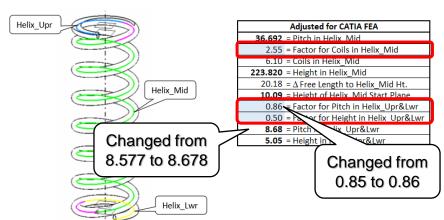
$$k = \frac{d^4G}{8D^3N_a}$$
 $v = \frac{E}{G \cdot 2} - 1$; $G = E / (2*(1+v))$

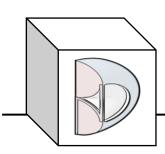
Calculated Pitch [P]				ring Outer meter [OD			ring Inner meter [ID]	Spring rate [k]		
inch	m	mm	inch	m	mm	inch	m	mm	lb/in	N/mm
1.411	0.0358	35.836	3.500	0.0889	88.9	2.500	0.0635	63.5	500.45	87.64

Spring Results (FEA)									
Mean Dia.	Force	defl	Rate						
mm	Ν	δ (mm)	(k) N/mm						
76.2	876.4	10	87.6						
	II.		H. P.						

in	lb	in	lb/in	
3.000	197.03	0.394	500.4	

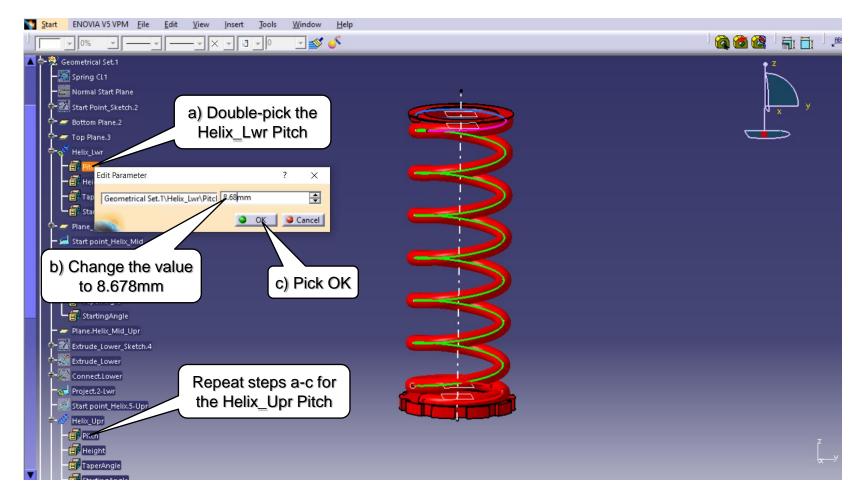


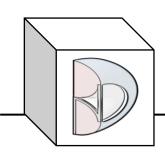






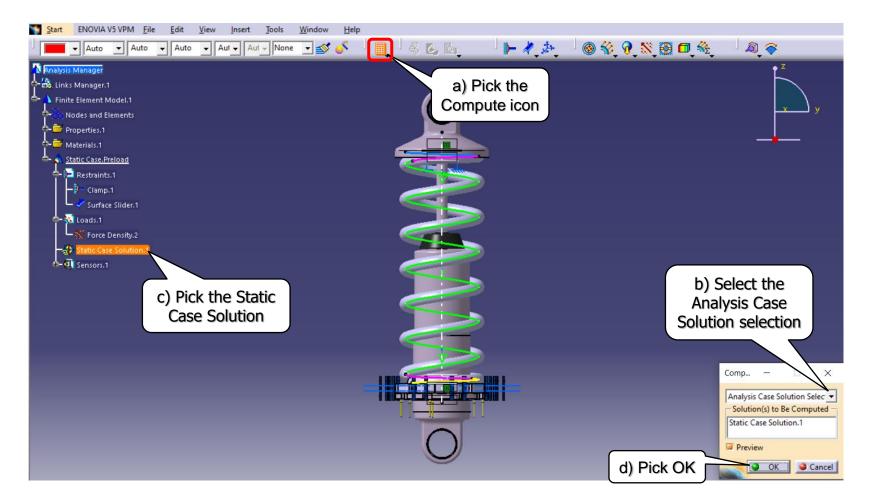
Adjust the Spring CATPart Upr & Lwr Helix.

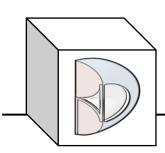






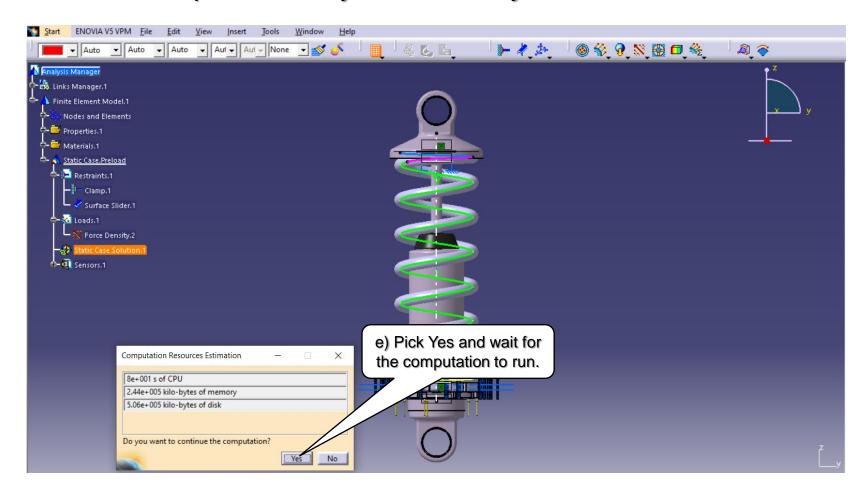
Re-compute the Assy Preload analysis.

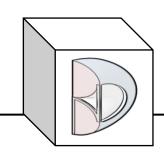






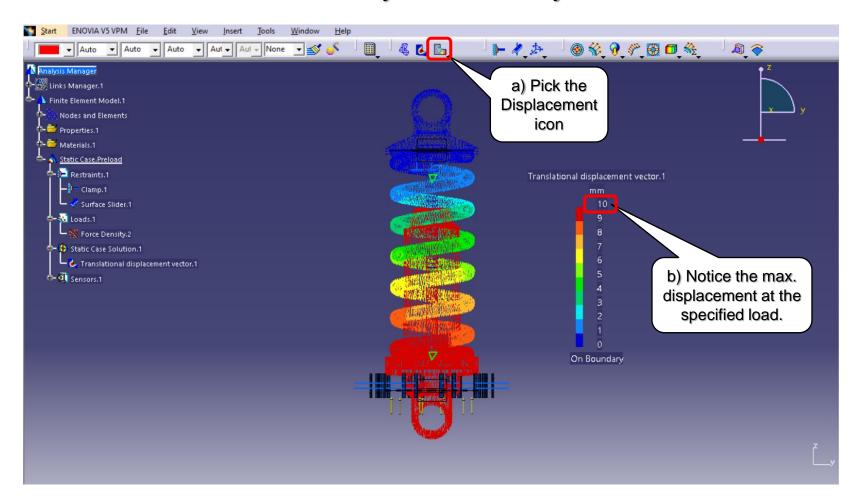
Re-compute the Assy Preload analysis.

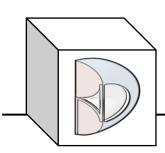






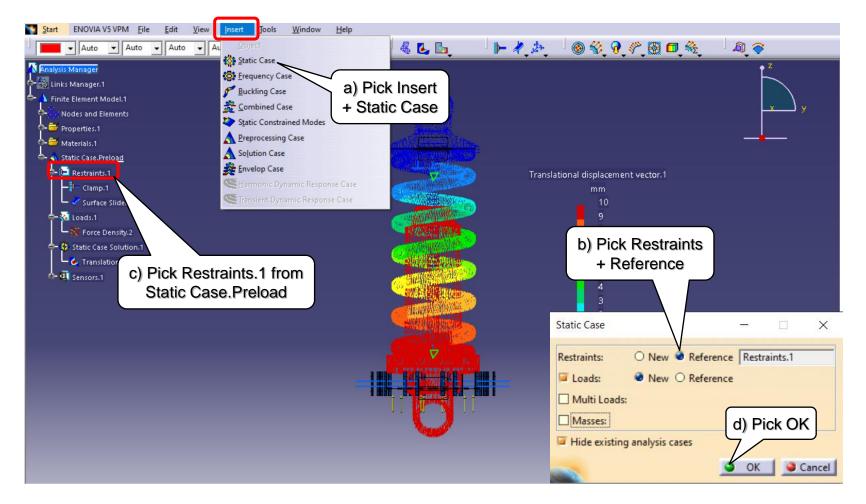
Show results of the Assy Preload analysis.

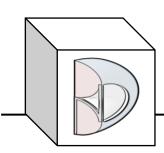






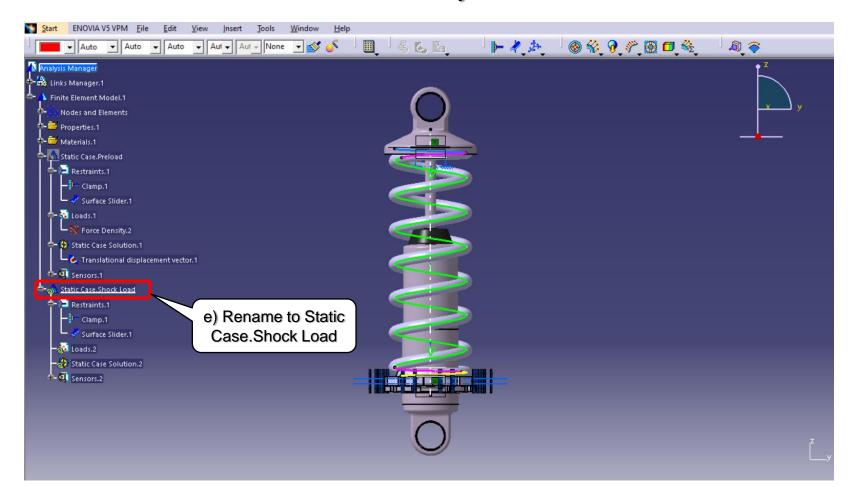
Create a new Static Case. Assy Shock Deflection.

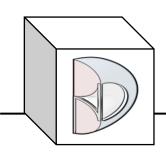






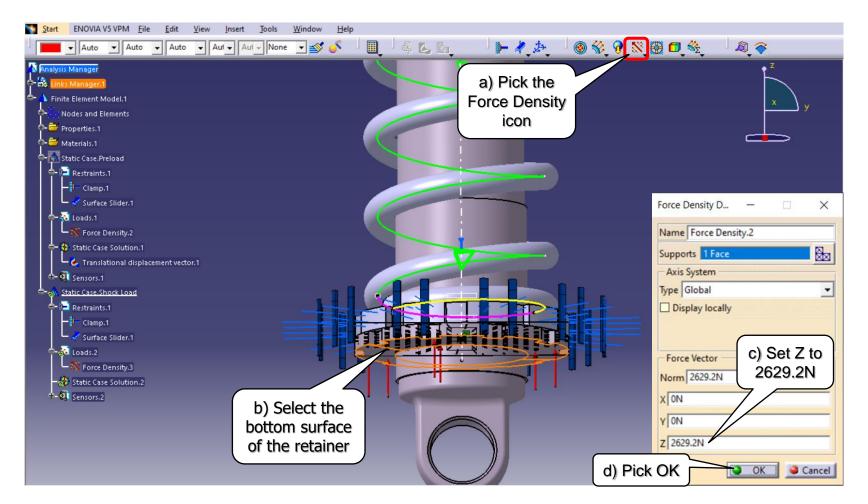
Create a new Static Case. Assy Shock Deflection.

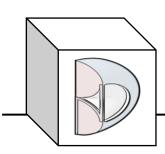






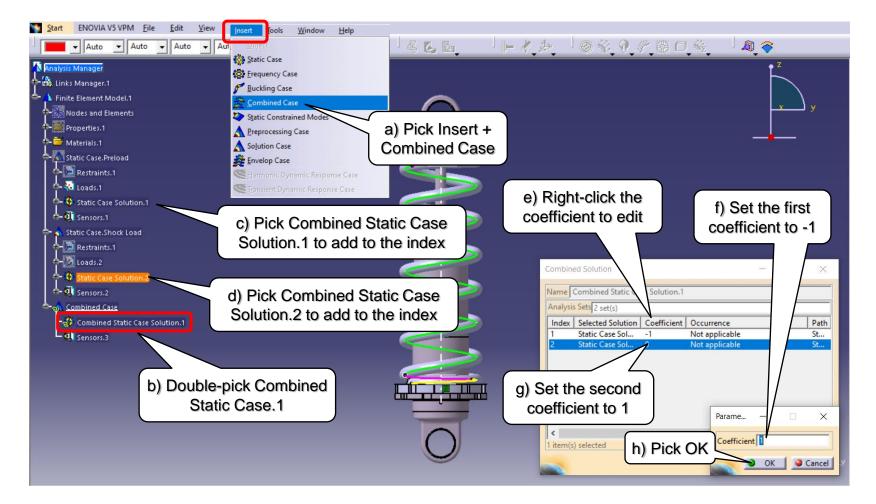
Create the new Shock Load (30 x rate → 2629.2N).

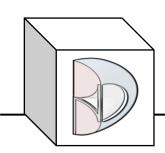






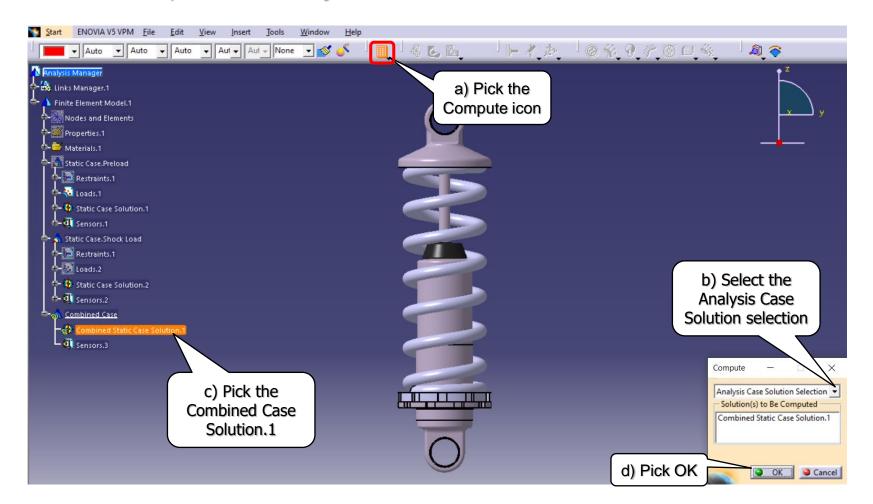
Create a new Combined Case. Assy Shock Deflection.

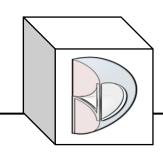






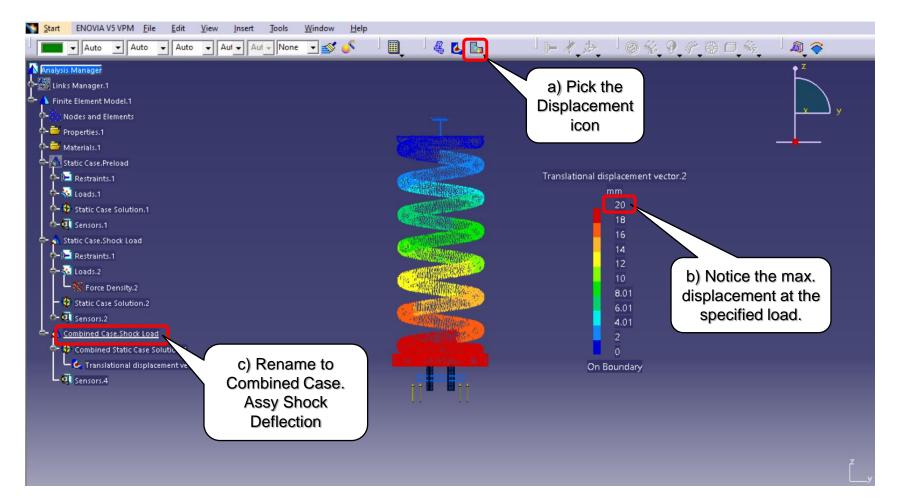
Compute the analysis for the Combined Case.

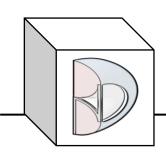






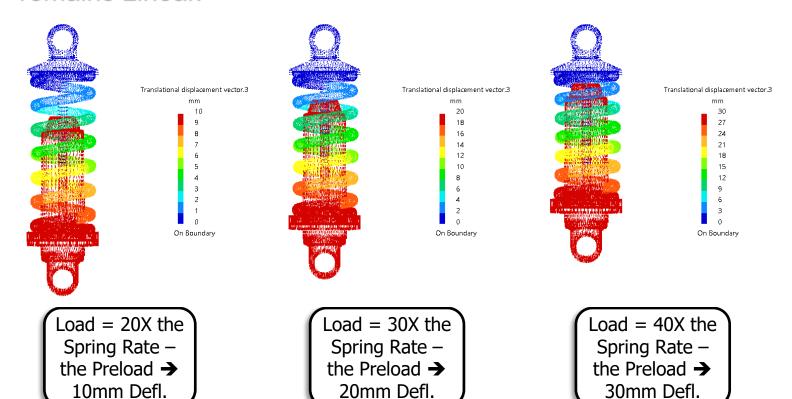
Show results of the analysis of the Combined Case. Assy Shock Deflection.

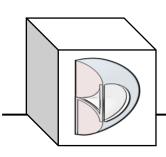






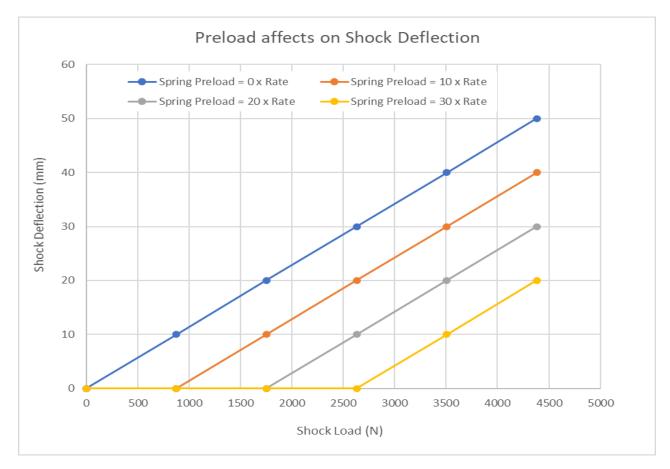
 The FEA analysis of the <u>Preloaded</u> Shock Assy correlates with the Spring Rate from the CATIA Part model and proves the rate remains Linear.

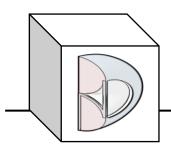






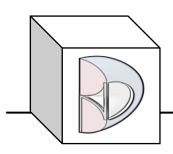
 Graph below shows the Shock Deflection based on Shock Load at various Preload conditions.







- In this Shock Absorber Preload Analysis, we have proven the following:
 - 1. The spring rate will be linear when the spring has a consistent (evenly spaced) pitch and a constant diameter.
 - Preloading the spring on the coil over assembly will NOT change the rate of the spring.
 - Preloading the spring on the coil over assembly WILL affect the deflection at load (length at load) of the shock absorber.





Conclusion:

This is an example of how to use CATIA Generative Structural Analysis to prove the affects of Preload within the coil over shock absorber.

We hope this analysis proves useful for those who need to show a Torsion Bar Analysis.

As always, we are open to any discussions this may bring.

Please *subscribe* to our YouTube channel!